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WOOD TRUSSES

STRESS COEFFICIENTS
LENGTH COEFFICIENTS
&
ANGLES

A
NATIONAL LUMBER MANUFACTURERS ASSOCIATION
PUBLICATION

1937

For a truss within the limitations stated, the total stress in any member, the length of any member between joint centers, and the angle between any two members may readily be found from the tables of coefficients given herein. This information was prepared by Frank J. Hanrahan and Mary C. Ahern.

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GLOSSARY OF TERMS

The following terms are defined in the limited sense in which they are used in this publication:

"Panel point load" is the exterior load applied at any one joint of the top or bottom chord of a truss.

"Joint" is any point in a truss where two or more members meet.

"Panel length" is the distance between any two consecutive joint centers in either the top or bottom chords.

"Joint center" is the point of intersection of the center lines of all the members meeting at any one joint.

"Top chord" is the one or more members which form the upper boundary of the truss.

"Bottom chord" is the one or more members which form the lower boundary of the truss.

"Member" is the aggregate of one or more pieces of structural material which lie between any two adjacent joints of a truss.

"Chord member" is a member which forms part of either the top or bottom chords.

"Web member" is a member which lies between the top and bottom chords.

"Stress coefficient" is a numerical constant which, when multiplied by the panel point load, gives the total axial stress in a truss member.

"Length coefficient" is a numerical constant which, when multiplied by the height of truss, gives the length of a truss member between joint centers.

"Pitch" is the ratio of "height of truss" to "span length" $\frac{H}{L} = \frac{1}{n}$ when both are expressed in the same linear units.

"Height of truss" is the vertical distance at mid-span from the joint center at the ridge of a pitched truss, or from the center line of the top chord of a flat truss, to the center line of the bottom chord.

"Span length" is the horizontal distance between the joint centers of the two joints located at the extreme ends of the truss.

LIMITATIONS

The stress coefficients in the tables are based on the assumptions that:

1. All loads act vertically. Non-vertical loads must be converted to assumed vertical loads or the axial stress in the member caused by such loads must be found by other means.
2. Load is applied to the truss at panel points only. The axial stresses (but not the additional bending stresses) induced in the members by uniformly distributed inter-panel point loads may be found by converting such loads to panel point loads and using the stress coefficients given.
3. The lengths of all panels comprising any one loaded chord are equal.
4. All panel point loads on any one chord are equal; with the exception that:
 - (a) For all except the top chord loadings of the Warren trusses, the panel point load at an end joint is one-half of that at an intermediate joint.
 - (b) For the top chord loadings of Warren trusses:
 - (1) the panel point load of an end joint is one-fourth, and at the joint next to the end is three-fourths of that at an intermediate joint, and
 - (2) the length of the end panel is one-half of that of an intermediate panel.

This represents the common loading when all vertical roof or ceiling loads are brought to the truss by means of purlins or beams located at panel points.

NOTATIONS

- H - height of truss in feet or inches.
- L - span length of truss in feet or inches.
- n - the ratio of "span length" to "height of truss" with height and span expressed in the same units; i.e., either feet or inches.
- N - A frequently repeated combination of mathematical terms which, for convenience in computation, has been given a special notation. (It does not necessarily represent the same mathematical expression for the different types of trusses).
- P - The panel point load applied at a joint of the top chord.
- p - The panel point load applied at a joint of the bottom chord.
- C - Center line about which the truss is symmetrical.
- ①, ②, ③, etc. on the sketch, and 1, 2, 3, etc. under column heading "member" in the table, designate individual members of the truss.

USE OF TABLES

Stress coefficients, length coefficients, and angles of members, for any one type of truss with a given number of panels, are shown on the same sheet. Conversion tables which will assist in converting inches and fractions of an inch to decimals of a foot, and fractions of an inch to decimals of an inch, are given on the last page of this manual.

Values of n , P , and p

Select type of truss and ratio of "span length" to "height of truss", N . In subsequent computations, use coefficients and angles in the vertical columns under "value of N " chosen. If a "value of N ", other than those given on the table, is desired, compute the coefficients and angles from the "General Formulas" in the columns at the extreme right of the tables. Since the pitch of a true Belgian truss is fixed by the number of panels, only one "value of N " is possible for each Belgian truss.

Determine the top and bottom panel point loads P and p by standard principles of mechanics.

Stress Coefficients

To find the total axial tensile or compressive stress in any member when the truss is loaded at:

1. TOP - Multiply P by the stress coefficient in the column under P .
2. BOTTOM - Multiply p by the stress coefficient in the column under p .
3. TOP AND BOTTOM - Add stresses determined in 1 and 2 above.

ALL MEMBERS WHICH ARE IN COMPRESSION MUST BE DESIGNED AS COLUMNS.

Members in compression are designated by heavy lines on the sketch and by minus signs before the tabulated stress coefficients.

Length of Members

To find the length of any member between joint centers, multiply H , the height of the truss, by the length coefficient under H .

Angles Between Members

The angles in degrees between members for use in determining bolt and connector loads, can be taken directly from the table; e.g., 1 - 9 under column heading "Members" indicates that the angle is measured between member ① and member ⑨ shown on the sketch.

Reactions

For each truss the gross reaction, i.e., the total vertical load which the wall or column supporting one end of the truss must carry, is shown on the sketch of the truss. If the rafters or ceiling joists rest directly on the wall, the loads used for determining the bearing areas at the ends of the truss should be modified accordingly.

Non-essential Truss Members

Members which are not essential for a complete truss, are shown on the sketches at the end of certain trusses by dotted lines. They are included to show possible variations in the shape of the truss.

In the Fink and Fan types of trusses, the vertical member at the center is not necessary for the stability of the truss, and therefore may be omitted if desired. In the larger spans it is customary to include this member to provide a center support for the central bottom chord member of the truss.

In the triangular Pratt and flat Howe trusses, the vertical member at the center may be omitted if there is no bottom chord load.

ADDITIONAL INFORMATION

Further information pertinent for truss design may be obtained from the National Lumber Manufacturers Association, and from the Regional Lumber Manufacturers Associations.

REFERENCES

"Wood Structural Design Data", National Lumber Manufacturers Association.

"Working Stresses for Structural Lumber", National Lumber Manufacturers Association

"Bolted Wood Joints - Safe Loads on Common Bolts", National Lumber Manufacturers Association.

"Maximum Spans for Joists and Rafters", National Lumber Manufacturers Association

"Wood Columns - Safe Loads", National Lumber Manufacturers Association

"Lumber Grade-Use Guide", National Lumber Manufacturers Association.

"Manual of Timber Connector Construction", Timber Engineering Company, Washington, D.C.

"Wood Handbook", (Forest Products Laboratory), U.S. Dept. of Agriculture.

"Wood Construction", by National Committee on Wood Utilization, McGraw-Hill Book Company.

"Wood Construction", by Voss and Varney, John Wiley & Sons.

"Timber Design and Construction", by Jacoby and Davis, John Wiley & Sons.

"Architects' and Builders' Handbook" by Kidder and Parker, John Wiley & Sons.

"Building Code", recommended by the National Board of Fire Underwriters.

"Uniform Building Code", recommended by the Pacific Coast Building Officials Conference.

"Douglas Fir Use Book - Structural Data and Design Tables", West Coast Lumbermen's Association.

"Southern Pine Manual of Standard Wood Construction", Southern Pine Association.

"Wood Bridges and Trestles", Reports of Committee VII, American Railway Engineering Association.

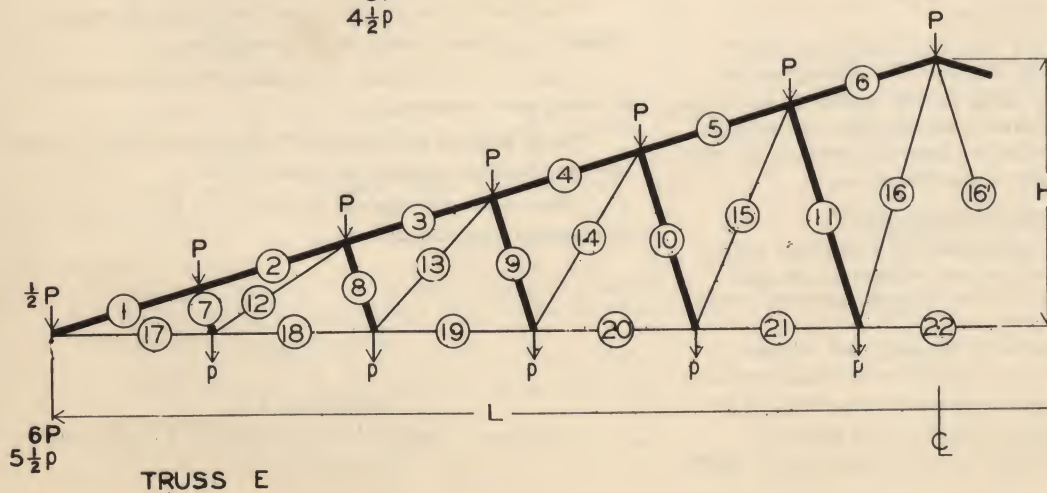
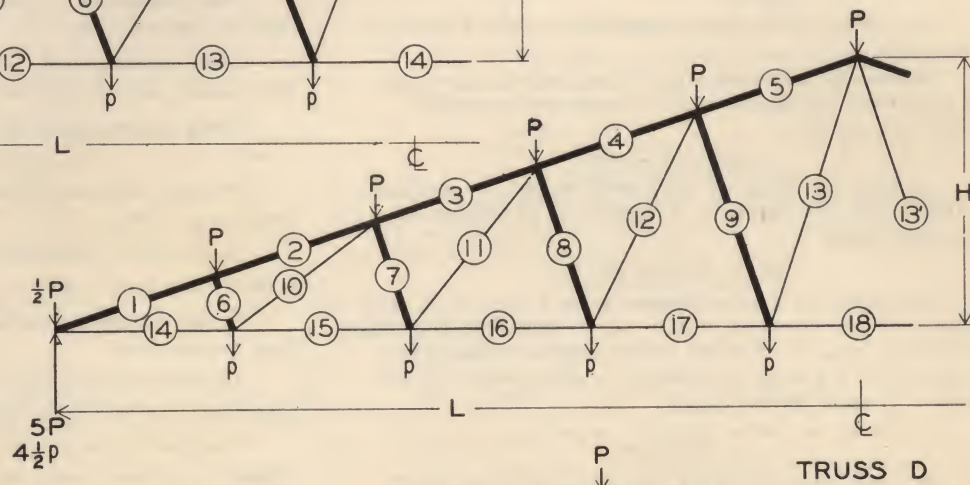
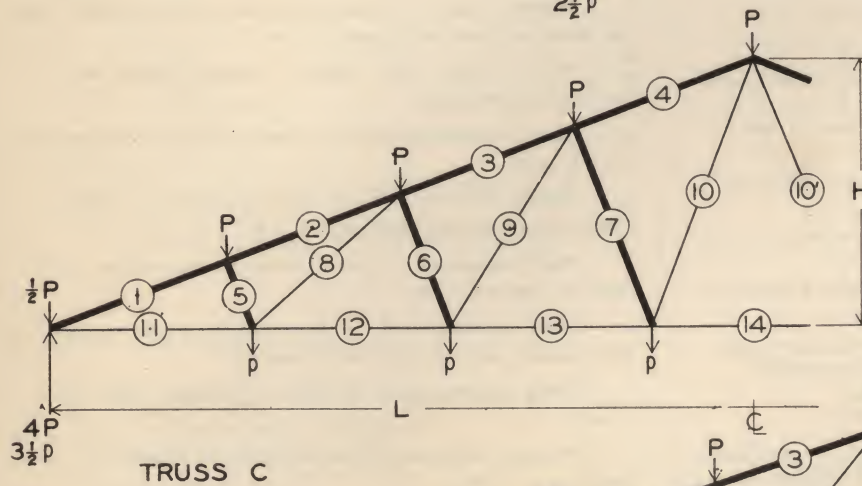
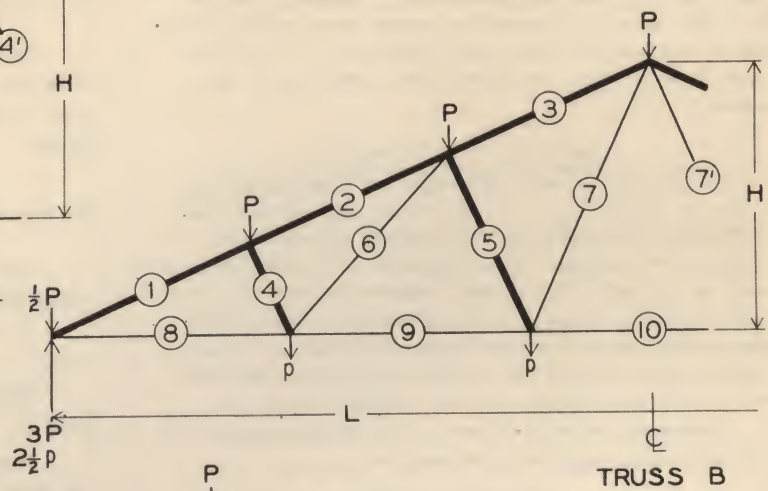
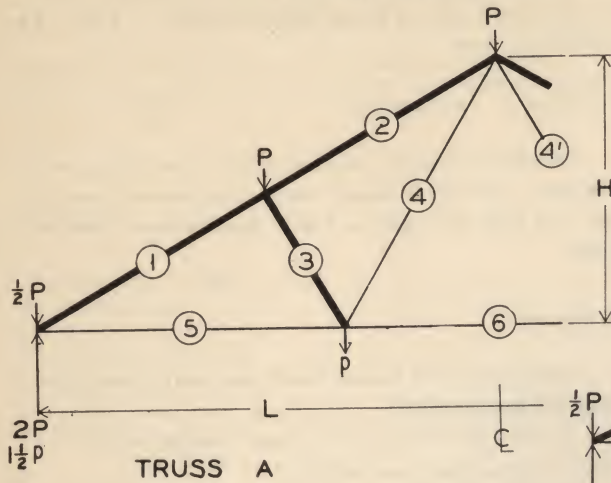
"Structural Members and Connections" by Hool & Kinne, McGraw-Hill Book Company.

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WASHINGTON, D.C.

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS & ANGLES - TRIANGULAR BELGIAN

ONE PANEL LESS AT BOTTOM THAN AT TOP



TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - TRIANGULAR BELGIAN

ONE PANEL LESS AT BOTTOM THAN AT TOP

To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P .
2. BOTTOM - multiply the panel point load p by the stress coefficient under p .
3. TOP & BOTTOM - add stresses determined in 1 and 2 above.

ALL MEMBERS WHICH ARE IN COMPRESSION MUST BE DESIGNED AS COLUMNS.

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| TRUSS A | TRUSS B | TRUSS C | TRUSS D | TRUSS E |
|--|---|---|---|---|
| Pitch = $H/L = 1/6 \sqrt{3}$ $n = L/H = 2 \sqrt{3} = 3.4642$ Roof Slope = $30^\circ 00'$ | Pitch = $H/L = 1/10 \sqrt{5}$ $n = L/H = 2 \sqrt{5} = 4.4722$ Roof Slope = $24^\circ 07'$ | Pitch = $H/L = 1/14 \sqrt{7}$ $n = L/H = 2 \sqrt{7} = 5.2915$ Roof Slope = $20^\circ 42'$ | Pitch = $H/L = 1/6$ $n = L/H = 6$ Roof Slope = $18^\circ 26'$ | Pitch = $H/L = 1/22 \sqrt{11}$ $n = L/H = 2 \sqrt{11} = 6.6332$ Roof Slope = $16^\circ 47'$ |

STRESS COEFFICIENTS

| MEMBER | P | p | MEMBER | P | p | MEMBER | P | p | MEMBER | P | p | MEMBER | P | p |
|--------|-------|-------|--------|-------|-------|--------|-------|-------|--------|--------|--------|--------|--------|--------|
| 1 | -3.00 | -2.00 | 1 | -6.12 | -4.90 | 1 | -9.90 | -8.48 | 1 | -14.23 | -12.65 | 1 | -19.06 | -17.32 |
| 2 | -2.50 | -2.00 | 2 | -5.72 | -4.90 | 2 | -9.55 | -8.48 | 2 | -13.91 | -12.65 | 2 | -18.76 | -17.32 |
| 3 | -0.87 | 0 | 3 | -4.29 | -3.67 | 3 | -7.95 | -7.07 | 3 | -12.17 | -11.07 | 3 | -16.89 | -15.59 |
| 4 | 0.87 | 1.15 | 4 | -0.91 | 0 | 4 | -6.36 | -5.66 | 4 | -10.44 | -9.49 | 4 | -15.01 | -13.86 |
| 5 | 2.60 | 1.75 | 5 | -1.37 | -0.55 | 5 | -0.94 | 0 | 5 | -8.70 | -7.91 | 5 | -13.13 | -12.12 |
| 6 | 1.75 | 1.15 | 6 | 1.12 | 1.34 | 6 | -1.40 | -0.53 | 6 | -0.95 | 0 | 6 | -11.26 | -10.39 |
| | | | 7 | 1.37 | 1.64 | 7 | -1.87 | -1.07 | 7 | -1.42 | -0.53 | 7 | -0.96 | 0 |
| | | | 8 | 5.59 | 4.47 | 8 | 1.32 | 1.51 | 8 | -1.90 | -1.05 | 8 | -1.44 | -0.52 |
| | | | 9 | 4.47 | 3.58 | 9 | 1.55 | 1.77 | 9 | -2.37 | -1.58 | 9 | -1.91 | -1.04 |
| | | | 10 | 3.35 | 2.68 | 10 | 1.87 | 2.14 | 10 | 1.50 | 1.67 | 10 | -2.39 | -1.57 |
| | | | | | | 11 | 9.26 | 7.94 | 11 | 1.71 | 1.90 | 11 | -2.87 | -2.09 |
| | | | | | | 12 | 7.94 | 6.80 | 12 | 2.01 | 2.24 | 12 | 1.66 | 1.81 |
| | | | | | | 13 | 6.61 | 5.67 | 13 | 2.37 | 2.64 | 13 | 1.85 | 2.02 |
| | | | | | | 14 | 5.29 | 4.54 | 14 | 15.50 | 12.00 | 14 | 2.14 | 2.34 |
| | | | | | | | | | 15 | 12.00 | 10.67 | 15 | 2.49 | 2.71 |
| | | | | | | | | | 16 | 10.50 | 9.33 | 16 | 2.87 | 3.13 |
| | | | | | | | | | 17 | 9.00 | 8.00 | 17 | 18.24 | 16.58 |
| | | | | | | | | | 18 | 7.50 | 6.67 | 18 | 16.58 | 15.08 |
| | | | | | | | | | | | | 19 | 14.92 | 13.57 |
| | | | | | | | | | | | | 20 | 13.27 | 12.06 |
| | | | | | | | | | | | | 21 | 11.61 | 10.55 |
| | | | | | | | | | | | | 22 | 9.95 | 9.05 |

LENGTH COEFFICIENTS

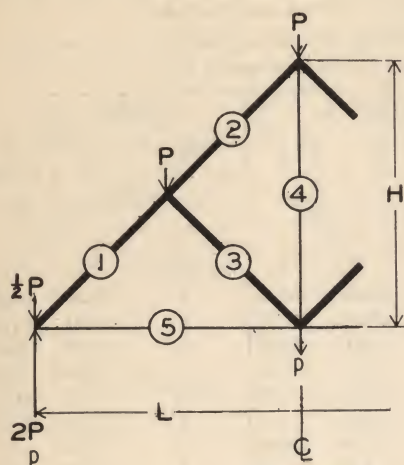
| MEMBER | H | MEMBER | H | MEMBER | H | MEMBER | H | MEMBER | H |
|---------|----------|----------|----------|-------------------|----------|------------------------|----------|----------------------------|----------|
| 1, 2 | 1.000000 | 1, 2, 3 | 0.816497 | 1, 2, 3, 4 | 0.707107 | 1, 2, 3, 4, 5, 8 | 0.632456 | 1, 2, 3, 4, 5, 8 | 0.577350 |
| 3 | 0.577350 | 4 | 0.365148 | 5 | 0.267261 | 6 | 0.210819 | 7 | 0.174078 |
| 4, 5, 6 | 1.154701 | 5 | 0.730296 | 6 | 0.534522 | 7 | 0.421637 | 8 | 0.348155 |
| | | 7 | 1.095445 | 7 | 0.801784 | 9 | 0.843274 | 9 | 0.522233 |
| | | 8, 9, 10 | 0.894427 | 8, 11, 12, 13, 14 | 0.755929 | 11 | 0.760117 | 10 | 0.696311 |
| | | | | 9 | 0.886405 | 12 | 0.894427 | 11 | 0.870388 |
| | | | | 10 | 1.069044 | 13 | 1.054092 | 12, 17, 18, 19, 20, 21, 22 | 0.603023 |
| | | | | | | 10, 14, 15, 16, 17, 18 | 0.666667 | 13 | 0.674200 |
| | | | | | | | | 14 | 0.778499 |
| | | | | | | | | 15 | 0.904534 |
| | | | | | | | | 16 | 1.044466 |

ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS

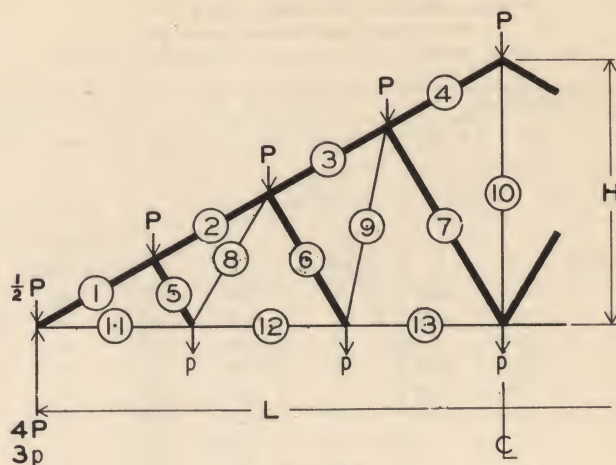
| MEMBER | DEG. | MEMBER | DEG. | MEMBER | DEG. | MEMBER | DEG. | MEMBER | DEG. |
|--------------------|------|--------------------------|------|----------------------------|------|------------------------------------|------|---|------|
| 1-5, 2-4 | 30 | 1-8, 2-6 | 24 | 1-11, 2-8 | 21 | 1-14, 2-10 | 18 | 1-17, 2-12 | 17 |
| 3-4, 3-5, 4-6, 4-4 | 60 | 3-7 | 42 | 3-9 | 37 | 3-11 | 34 | 3-13 | 31 |
| 1-3, 2-3 | 90 | 4-6, 4-8, 5-6, 5-9, 7-10 | 66 | 4-10 | 49 | 4-12, 8-12, 9-12 | 45 | 4-14 | 42 |
| | | 5-7, 6-9, 7-7 | 48 | 5-8, 5-11, 6-8, 6-12, 7-13 | 69 | 5-13 | 53 | 5-15 | 50 |
| | | 1-4, 2-4, 3-5 | 90 | 6-9, 7-9 | 53 | 6-10, 6-14, 7-10, 7-15, 8-16, 9-17 | 72 | 6-16 | 56 |
| | | | | 7-10 | 41 | 7-11, 8-11 | 56 | 7-12, 7-17, 8-12, 8-18, 9-19, 10-20, 11-21, 16-22 | 73 |
| | | | | 8-12 | 42 | 9-13 | 37 | 8-13, 9-13, 14-20 | 59 |
| | | | | 9-13 | 58 | 10-15 | 36 | 9-14, 10-14, 13-19 | 48 |
| | | | | 10-14 | 70 | 11-16 | 52 | 10-15, 11-15 | 40 |
| | | | | 1-5, 2-5, 3-6, 4-7 | 90 | 12-17 | 63 | 11-16, 12-18, 16-16 | 34 |
| | | | | 10-10 | 40 | 13-18 | 71 | 16-21 | 67 |
| | | | | | | 1-6, 2-6, 3-7, 4-8, 5-9 | 90 | 1-7, 2-7, 3-8, 4-9, 5-10, 6-11 | 90 |
| | | | | | | 13-13 | 58 | | |

TRUSSES- STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - TRIANGULAR BELGIAN

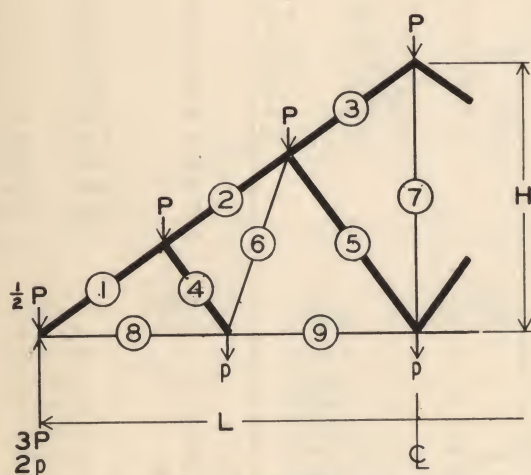
TWO PANELS LESS AT BOTTOM THAN AT TOP



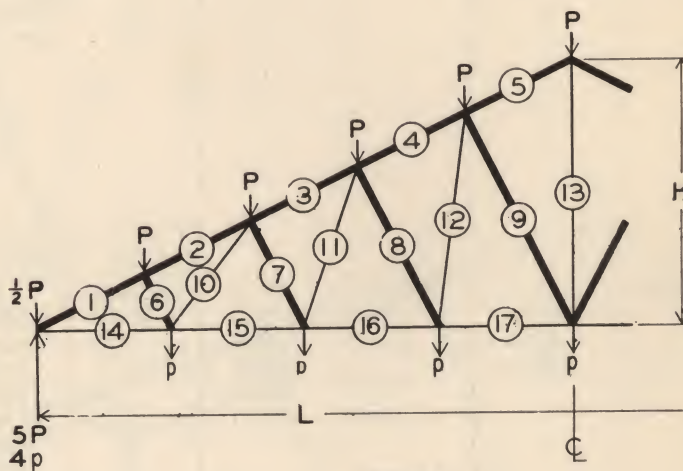
TRUSS F



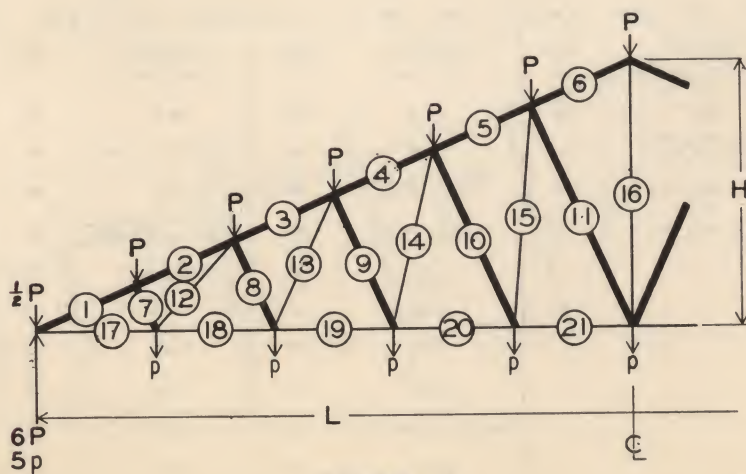
TRUSS H



TRUSS G



TRUSS I



TRUSS J

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - TRIANGULAR BELGIAN

TWO PANELS LESS AT BOTTOM THAN AT TOP

To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P .
2. BOTTOM - multiply the panel point load p by the stress coefficient under p .
3. TOP & BOTTOM - add stresses determined in 1 and 2 above.

ALL MEMBERS WHICH ARE IN COMPRESSION MUST BE DESIGNED AS COLUMNS.

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| TRUSS F | TRUSS G | TRUSS H | TRUSS I | TRUSS J |
|---|--|--|---|---|
| Pitch = $H/L = 1/2$ $n = L/H = 2$ Roof Slope = 45° | Pitch = $H/L = 1/4 \sqrt{2}$ $n = L/H = 2 \sqrt{2} = 2.8284$ Roof Slope = $35^\circ 16'$ | Pitch = $H/L = 1/6 \sqrt{3}$ $n = L/H = 2 \sqrt{3} = 3.4642$ Roof Slope = 30° | Pitch = $H/L = 1/4$ $n = L/H = 4$ Roof Slope = $26^\circ 34'$ | Pitch = $H/L = 1/10 \sqrt{5}$ $n = L/H = 2 \sqrt{5} = 4.4722$ Roof Slope = $24^\circ 07'$ |

STRESS COEFFICIENTS

| MEMBER | P | p | MEMBER | P | p | MEMBER | P | p | MEMBER | P | p | MEMBER | P | p |
|--------|-------|-------|--------|-------|-------|--------|-------|-------|--------|--------|-------|--------|--------|--------|
| 1 | -2.12 | -0.71 | 1 | -4.33 | -2.60 | 1 | -7.00 | -5.00 | 1 | -10.06 | -7.83 | 1 | -13.47 | -11.02 |
| 2 | -1.41 | -0.71 | 2 | -5.75 | -2.60 | 2 | -6.50 | -5.00 | 2 | -9.62 | -7.83 | 2 | -13.06 | -11.02 |
| 3 | -0.71 | 0 | 3 | -2.60 | -1.73 | 3 | -5.25 | -4.00 | 3 | -8.27 | -6.71 | 3 | -11.64 | -9.80 |
| 4 | 1.00 | 1.00 | 4 | -0.82 | 0 | 4 | -4.00 | -3.00 | 4 | -6.93 | -5.59 | 4 | -10.21 | -8.57 |
| 5 | 1.50 | 0.50 | 5 | -1.22 | -0.61 | 5 | -0.87 | 0 | 5 | -5.59 | -4.47 | 5 | -8.78 | -7.35 |
| | | | 6 | 0.71 | 1.06 | 6 | -1.30 | -0.57 | 6 | -0.89 | 0 | 6 | -7.35 | -6.12 |
| | | | 7 | 2.00 | 2.00 | 7 | -1.73 | -1.15 | 7 | -1.54 | -0.56 | 7 | -0.91 | 0 |
| | | | 8 | 3.54 | 2.12 | 8 | 0.87 | 1.15 | 8 | -1.79 | -1.13 | 8 | -1.37 | -0.55 |
| | | | 9 | 2.83 | 1.77 | 9 | 1.15 | 1.53 | 9 | -2.24 | -1.68 | 9 | -1.83 | -1.10 |
| | | | | | | 10 | 3.00 | 3.00 | 10 | 1.00 | 1.25 | 10 | -2.28 | -1.64 |
| | | | | | | 11 | 6.06 | 4.33 | 11 | 1.26 | 1.68 | 11 | -2.74 | -2.19 |
| | | | | | | 12 | 5.20 | 3.75 | 12 | 1.61 | 2.02 | 12 | 1.12 | 1.54 |
| | | | | | | 13 | 4.33 | 3.18 | 13 | 4.00 | 4.00 | 13 | 1.37 | 1.64 |
| | | | | | | | | | 14 | 9.00 | 7.00 | 14 | 1.71 | 2.06 |
| | | | | | | | | | 15 | 8.00 | 6.25 | 15 | 2.09 | 2.51 |
| | | | | | | | | | 16 | 7.00 | 5.50 | 16 | 5.00 | 5.00 |
| | | | | | | | | | 17 | 6.00 | 4.75 | 17 | 12.30 | 10.06 |
| | | | | | | | | | | | | 18 | 11.18 | 9.17 |
| | | | | | | | | | | | | 19 | 10.06 | 8.27 |
| | | | | | | | | | | | | 20 | 8.94 | 7.38 |
| | | | | | | | | | | | | 21 | 7.83 | 6.48 |

LENGTH COEFFICIENTS

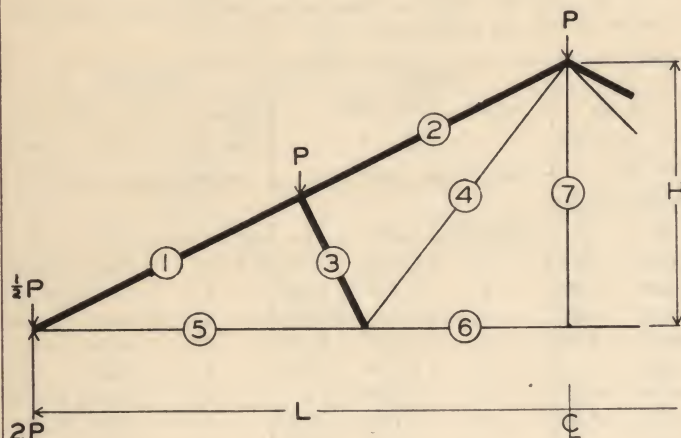
| MEMBER | H | MEMBER | H | MEMBER | H | MEMBER | H | MEMBER | H |
|---------|----------|---------|----------|------------------|----------|--------------------|----------|------------------------|----------|
| 1, 2, 3 | 0.707107 | 1, 2, 3 | 0.577344 | 1, 2, 3, 4 | 0.500000 | 1, 2, 3, 4, 5, 7 | 0.447214 | 1, 2, 3, 4, 5, 6 | 0.408248 |
| 4, 5 | 1.000000 | 4 | 0.408248 | 5 | 0.288675 | 6 | 0.223607 | 7 | 0.182574 |
| | | 5 | 0.816497 | 6, 8, 11, 12, 13 | 0.577350 | 8 | 0.670820 | 8 | 0.365149 |
| | | 6, 8, 9 | 0.707107 | 7 | 0.866025 | 9 | 0.894427 | 9, 13 | 0.547723 |
| | | 7 | 1.000000 | 9 | 0.763763 | 10, 14, 15, 16, 17 | 0.500000 | 10 | 0.730297 |
| | | | | 10 | 1.000000 | 11 | 0.632456 | 11 | 0.912871 |
| | | | | | | 12 | 0.806226 | 12, 17, 18, 19, 20, 21 | 0.447214 |
| | | | | | | 13 | 1.000000 | 14 | 0.683130 |
| | | | | | | | | 15 | 0.836660 |
| | | | | | | | | 16 | 1.000000 |

ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS

| MEMBER | DEG. | MEMBER | DEG. | MEMBER | DEG. | MEMBER | DEG. | MEMBER | DEG. |
|--------------------|------|-------------------------|------|--|------|------------------------------------|------|---|------|
| 1-5, 2-4, 3-4, 3-5 | 45 | 1-8, 2-6, 5-7 | 35 | 1-11, 2-8, 7-10 | 30 | 1-14, 2-10, 9-13 | 27 | 1-17, 2-12, 11-16 | 24 |
| 1-3, 2-3 | 90 | 3-7, 4-6, 4-8, 5-6, 5-9 | 55 | 3-9 | 49 | 3-11, 7-11, 8-11 | 45 | 3-13 | 42 |
| | | 6-9 | 70 | 4-10, 5-8, 5-11, 6-8, 6-12, 7-13, 8-12 | 60 | 4-12 | 56 | 4-14 | 53 |
| | | 1-4, 2-4, 3-5 | 90 | 6-9, 7-9 | 41 | 5-13, 6-10, 7-10, 7-15, 8-16, 9-17 | 63 | 5-15 | 61 |
| | | | | 9-13 | 79 | 8-12, 9-12 | 34 | 6-16, 7-12, 7-17, 8-12, 8-16, 9-16, 10-20, 11-21, 13-19 | 66 |
| | | | | 1-5, 2-5, 3-6, 4-7 | 90 | 10-15 | 54 | 8-13, 9-13, 12-18 | 48 |
| | | | | | | 11-16 | 72 | 9-14, 10-14 | 37 |
| | | | | | | 12-17 | 83 | 10-15, 11-15 | 29 |
| | | | | | | 1-6, 2-6, 3-7, 4-8, 5-9 | 90 | 14-20 | 77 |
| | | | | | | | | 15-21 | 85 |
| | | | | | | | | 1-7, 2-7, 3-8, 4-9, 5-10, 6-11 | 90 |

TRUSSES STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - TRIANGULAR FINK

4 PANELS AT TOP



$$\text{PITCH} = \frac{H}{L} = \frac{1}{n}$$

$$n = \frac{L}{H}$$

$$N = \sqrt{n^2 + 4}$$

To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P

ALL MEMBERS WHICH ARE IN COMPRESSION MUST BE DESIGNED AS COLUMNS

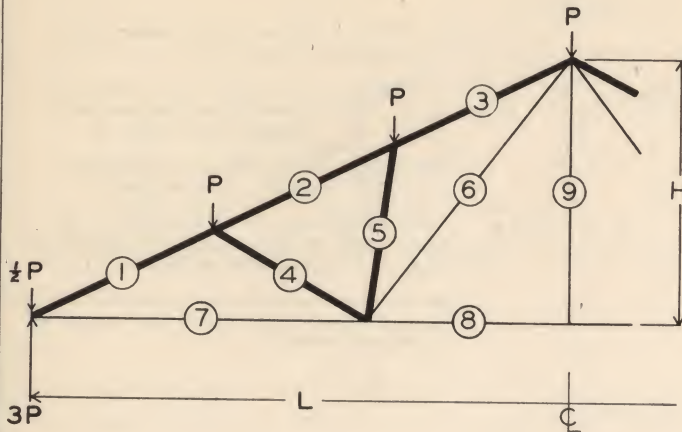
Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | GENERAL FORMULAS |
|---|---------------|----------|-------------|----------|----------|----------|----------|----------------------|
| | 2 | 3 | $2\sqrt{3}$ | 4 | 5 | 6 | 7 | |
| STRESS COEFFICIENTS | | | | | | | | |
| | P | P | P | P | P | P | P | P |
| 1 | -2.12 | -2.70 | -3.00 | -3.35 | -4.04 | -4.74 | -5.46 | $-3/4 N$ |
| 2 | -1.41 | -2.15 | -2.50 | -2.91 | -3.67 | -4.43 | -5.19 | $-1/N (3/4 n^2 + 1)$ |
| 3 | -0.71 | -0.83 | -0.87 | -0.89 | -0.93 | -0.95 | -0.96 | $-n/N$ |
| 4 | 0.50 | 0.75 | 0.87 | 1.00 | 1.25 | 1.50 | 1.75 | $1/4 n$ |
| 5 | 1.50 | 2.25 | 2.60 | 3.00 | 3.75 | 4.50 | 5.25 | $3/4 n$ |
| 6 | 1.00 | 1.50 | 1.73 | 2.00 | 2.50 | 3.00 | 3.50 | $1/2 n$ |
| 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| LENGTH COEFFICIENTS | | | | | | | | |
| | H | H | H | H | H | H | H | H |
| 1, 2 | 0.707107 | 0.901388 | 1.000000 | 1.118034 | 1.346291 | 1.581139 | 1.820027 | $1/4 N$ |
| 3 | 0.707107 | 0.600925 | 0.577357 | 0.559017 | 0.538516 | 0.527046 | 0.520008 | $1/2 N/n$ |
| 4, 5 | 1.000000 | 1.083333 | 1.154734 | 1.250000 | 1.450000 | 1.666667 | 1.892857 | $1/4 N^2/n$ |
| 6 | 0.000000 | 0.416667 | 0.577250 | 0.750000 | 1.050000 | 1.333333 | 1.607143 | $1/4 (n - 4/n)$ |
| 7 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | |
| 1-5, 2-4 | 45 | 34 | 30 | 27 | 22 | 18 | 16 | $2/n = \tan a$ |
| 4-6 | 90 | 68 | 60 | 54 | 44 | 36 | 32 | $2a$ |
| 3-4, 3-5 | 45 | 56 | 60 | 63 | 68 | 72 | 74 | $90 - a$ |
| 4-7 | 0 | 22 | 30 | 36 | 46 | 54 | 58 | $90 - 2a$ |
| 1-3, 2-3, 6-7 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - TRIANGULAR FAN

6 PANELS AT TOP



$$\text{PITCH} = \frac{H}{L} = \frac{1}{n}$$

$$n = \frac{L}{H}$$

$$N = \sqrt{n^2 + 4}$$

To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P

ALL MEMBERS WHICH ARE IN COMPRESSION MUST BE DESIGNED AS COLUMNS

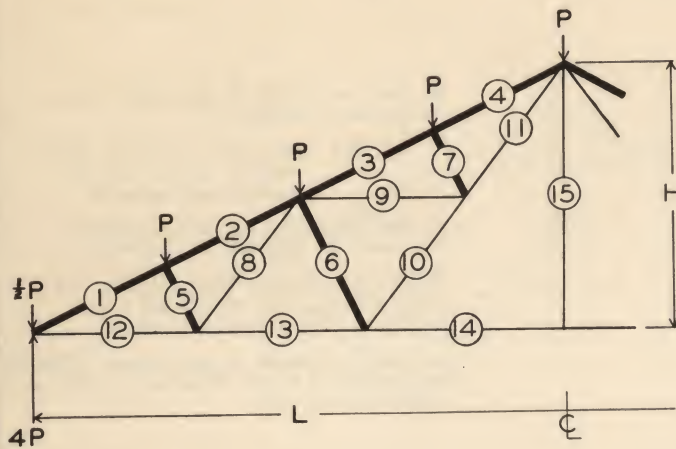
Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | GENERAL FORMULAS |
|---|-------------|----------|----------|----------|----------|----------|----------|------------------------------------|
| | 2 | 3 | 2√3 | 4 | 5 | 6 | 7 | |
| STRESS COEFFICIENTS | | | | | | | | |
| | P | P | P | P | P | P | P | P |
| 1 | -3.54 | -4.51 | -5.00 | -5.59 | -6.73 | -7.91 | -9.10 | - 5/4 N |
| 2 | -2.59 | -3.54 | -4.00 | -4.55 | -5.59 | -6.64 | -7.70 | - 13 N ² - 16 12 N |
| 3 | -2.12 | -3.40 | -4.00 | -4.70 | -5.99 | -7.27 | -8.55 | - 5 n ³ + 4 4 N |
| 4 | -0.75 | -0.93 | -1.00 | -1.07 | -1.21 | -1.34 | -1.48 | - n √n ² + 36 6 N |
| 5 | -0.75 | -0.93 | -1.00 | -1.07 | -1.21 | -1.34 | -1.48 | - n √n ² + 36 6 N |
| 6 | 1.00 | 1.50 | 1.73 | 2.00 | 2.50 | 3.00 | 3.50 | 1/2 n |
| 7 | 2.50 | 3.75 | 4.33 | 5.00 | 6.25 | 7.50 | 8.75 | 5/4 n |
| 8 | 1.50 | 2.25 | 2.60 | 3.00 | 3.75 | 4.50 | 5.25 | 3/4 n |
| 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| LENGTH COEFFICIENTS | | | | | | | | |
| | H | H | H | H | H | H | H | H |
| 1, 2, 3 | 0.471405 | 0.600925 | 0.666667 | 0.745356 | 0.897527 | 1.054093 | 1.213352 | 1/6 N |
| 4, 5 | 0.745356 | 0.671855 | 0.666666 | 0.671855 | 0.700991 | 0.745356 | 0.799039 | 1/12 N (√n ² + 36) n |
| 6, 7 | 1.000000 | 1.085333 | 1.154734 | 1.250000 | 1.450000 | 1.666667 | 1.892857 | 1/4 N ² /n |
| 8 | 0.000000 | 0.416667 | 0.577250 | 0.750000 | 1.050000 | 1.333333 | 1.607150 | 1/4 (n - 4/n) |
| 9 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | |
| 1-7, 3-6 | 45 | 34 | 30 | 27 | 22 | 18 | 16 | 2/n = tan a |
| 2-4, 2-5 | 72 | 65 | 60 | 56 | 50 | 45 | 41 | 6/n = tan b |
| 6-8 | 90 | 68 | 60 | 54 | 44 | 36 | 32 | 2a |
| 6-9 | 0 | 22 | 30 | 36 | 46 | 54 | 58 | 90 - 2a |
| 4-7, 5-6 | 27 | 29 | 30 | 29 | 28 | 27 | 25 | b - a |
| 1-4, 3-5 | 108 | 117 | 120 | 124 | 130 | 135 | 139 | 180 - b |
| 4-5 | 36 | 54 | 60 | 68 | 80 | 90 | 98 | 180 - 2b |
| 8-9 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - TRIANGULAR FINK

8 PANELS AT TOP



$$\text{PITCH} = \frac{H}{L} = \frac{1}{n}$$

$$n = \frac{L}{H}$$

$$N = \sqrt{n^2 + 4}$$

To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P

ALL MEMBERS WHICH ARE IN COMPRESSION MUST BE DESIGNED AS COLUMNS

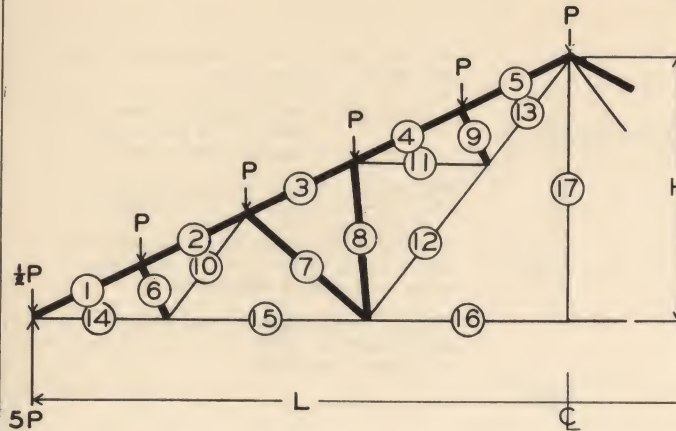
Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | GENERAL FORMULAS |
|---|-------------|----------|----------|----------|----------|----------|----------|-----------------------|
| | 2 | 3 | 2√3 | 4 | 5 | 6 | 7 | |
| STRESS COEFFICIENTS | | | | | | | | |
| | P | P | P | P | P | P | P | P |
| 1 | -4.96 | -6.31 | -7.00 | -7.83 | -9.42 | -11.07 | -12.74 | - 7/4 N |
| 2 | -4.24 | -5.76 | -6.50 | -7.38 | -9.05 | -10.75 | -12.47 | - (7/4 N - 2/N) |
| 3 | -3.54 | -5.20 | -6.00 | -6.93 | -8.68 | -10.43 | -12.19 | - (7/4 N - 4/N) |
| 4 | -2.83 | -4.65 | -5.50 | -6.48 | -8.31 | -10.12 | -11.92 | - (7/4 N - 6/N) |
| 5 | -0.71 | -0.83 | -0.87 | -0.89 | -0.93 | - 0.95 | - 0.96 | - n/N |
| 6 | -1.41 | -1.66 | -1.73 | -1.79 | -1.86 | - 1.90 | - 1.92 | - 2 n/N |
| 7 | -0.71 | -0.83 | -0.87 | -0.89 | -0.93 | - 0.95 | - 0.96 | - n/N |
| 8 | 0.50 | 0.75 | 0.87 | 1.00 | 1.25 | 1.50 | 1.75 | 1/4 n |
| 9 | 0.50 | 0.75 | 0.87 | 1.00 | 1.25 | 1.50 | 1.75 | 1/4 n |
| 10 | 1.00 | 1.50 | 1.73 | 2.00 | 2.50 | 3.00 | 3.50 | 1/2 n |
| 11 | 1.50 | 2.25 | 2.60 | 3.00 | 3.75 | 4.50 | 5.25 | 3/4 n |
| 12 | 3.50 | 5.25 | 6.06 | 7.00 | 8.75 | 10.50 | 12.25 | 7/4 n |
| 13 | 3.00 | 4.50 | 5.20 | 6.00 | 7.50 | 9.00 | 10.50 | 3/2 n |
| 14 | 2.00 | 3.00 | 3.46 | 4.00 | 5.00 | 6.00 | 7.00 | n |
| 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| LENGTH COEFFICIENTS | | | | | | | | |
| | H | H | H | H | H | H | H | H |
| 1, 2, 3, 4 | 0.353553 | 0.450694 | 0.500000 | 0.559017 | 0.673146 | 0.790569 | 0.910014 | 1/8 N |
| 5, 7 | 0.353553 | 0.300463 | 0.288684 | 0.279509 | 0.269258 | 0.263523 | 0.260004 | 1/4 N/n |
| 6 | 0.707107 | 0.600925 | 0.577357 | 0.559017 | 0.538516 | 0.527046 | 0.520008 | 1/2 N/n |
| 8, 9, 10, 11, 12, 13 | 0.500000 | 0.541667 | 0.577357 | 0.625000 | 0.725000 | 0.833333 | 0.946429 | 1/8 N ² /n |
| 14 | 0.000000 | 0.416667 | 0.577250 | 0.750000 | 1.050000 | 1.333333 | 1.607150 | 1/4 (n - 4/n) |
| 15 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | |
| 1-12, 2-3, 3-9, 4-11 | 45 | 34 | 30 | 27 | 22 | 18 | 16 | 2/n = tan a |
| 5-8, 6-12, 6-3, 6-9, 6-10, 6-13, 7-9, 7-11 | 45 | 56 | 60 | 63 | 68 | 72 | 74 | 90 - a |
| 8-13, 9-10, 10-14 | 90 | 68 | 60 | 54 | 44 | 36 | 32 | 2a |
| 11-15 | 0 | 22 | 30 | 36 | 46 | 54 | 58 | 90 - 2a |
| 1-5, 2-5, 3-7, 4-7, 14-15 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - TRIANGULAR FAN

10 PANELS AT TOP



$$\text{PITCH} = \frac{H}{L} = \frac{1}{n}$$

$$n = \frac{L}{H}$$

$$N = \sqrt{n^2 + 4}$$

To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P

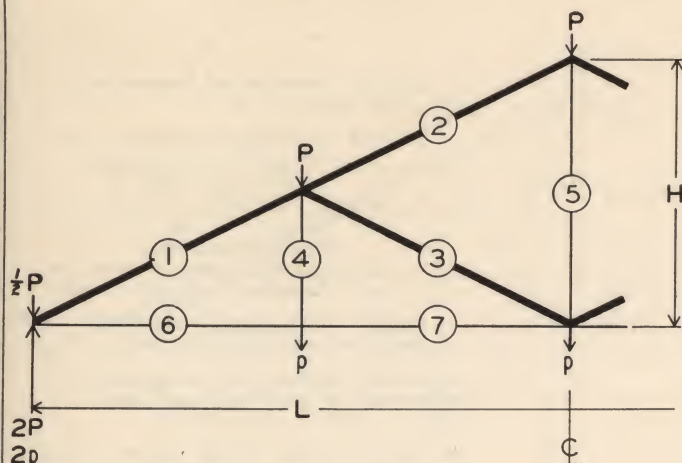
ALL MEMBERS WHICH ARE IN COMPRESSION MUST BE DESIGNED AS COLUMNS

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | GENERAL FORMULAS |
|---|-------------|----------|----------|----------|----------|----------|----------|------------------------------------|
| | 2 | 3 | 2√3 | 4 | 5 | 6 | 7 | |
| STRESS COEFFICIENTS | | | | | | | | |
| | P | P | P | P | P | P | P | P |
| 1 | -6.36 | -8.11 | -9.00 | -10.06 | -12.12 | -14.23 | -16.38 | - 9/4 N |
| 2 | -5.66 | -7.55 | -8.50 | - 9.62 | -11.75 | -13.91 | -16.11 | - 1/4 ($\frac{9n^2}{N} + 28$) |
| 3 | -4.37 | -6.00 | -6.80 | - 7.74 | - 9.52 | -11.31 | -13.14 | - 1/20 ($\frac{37n^2}{N} + 100$) |
| 4 | -4.24 | -6.44 | -7.50 | - 8.72 | -11.00 | -13.28 | -15.56 | - 3/4 ($\frac{3n^2}{N} + 4$) |
| 5 | -3.54 | -5.89 | -7.00 | - 8.27 | -10.63 | -12.97 | -15.28 | - 1/4 ($\frac{9n^2}{N} + 4$) |
| 6 | -0.71 | -0.83 | -0.87 | - 0.89 | - 0.93 | - 0.95 | - 0.96 | - n/N |
| 7 | -1.08 | -1.31 | -1.38 | - 1.44 | - 1.56 | - 1.66 | - 1.76 | - 3/20 n/N √n² + 100 |
| 8 | -1.08 | -1.31 | -1.38 | - 1.44 | - 1.56 | - 1.66 | - 1.76 | - 3/20 n/N √n² + 100 |
| 9 | -0.71 | -0.83 | -0.87 | - 0.89 | - 0.93 | - 0.95 | - 0.96 | - n/N |
| 10 | 0.50 | 0.75 | 0.87 | 1.00 | 1.25 | 1.50 | 1.75 | 1/4 n |
| 11 | 0.50 | 0.75 | 0.87 | 1.00 | 1.25 | 1.50 | 1.75 | 1/4 n |
| 12 | 1.50 | 2.25 | 2.60 | 3.00 | 3.75 | 4.50 | 5.25 | 3/4 n |
| 13 | 2.00 | 3.00 | 3.46 | 4.00 | 5.00 | 6.00 | 7.00 | n |
| 14 | 4.50 | 6.75 | 7.79 | 9.00 | 11.25 | 13.50 | 15.75 | 9/4 n |
| 15 | 4.00 | 6.00 | 6.92 | 8.00 | 10.00 | 12.00 | 14.00 | 2n |
| 16 | 2.50 | 3.75 | 4.34 | 5.00 | 6.25 | 7.50 | 8.75 | 5/4 n |
| 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| LENGTH COEFFICIENTS | | | | | | | | |
| | H | H | H | H | H | H | H | H |
| 1, 2, 3, 4, 5 | 0.282843 | 0.360555 | 0.400000 | 0.447214 | 0.538516 | 0.632456 | 0.728011 | 1/10 N |
| 6, 9 | 0.282843 | 0.240370 | 0.230947 | 0.223607 | 0.215407 | 0.210819 | 0.208003 | 1/5 N/n |
| 7, 8 | 0.721110 | 0.627384 | 0.611028 | 0.602080 | 0.602080 | 0.614636 | 0.634750 | 1/20 N/n √n² + 100 |
| 10, 11, 13, 14 | 0.400000 | 0.433333 | 0.461894 | 0.500000 | 0.580000 | 0.666667 | 0.757143 | 1/10 N²/n |
| 12, 15 | 0.600000 | 0.650000 | 0.692841 | 0.750000 | 0.870000 | 1.000000 | 1.135715 | 3/20 N²/n |
| 16 | 0.000000 | 0.416667 | 0.575000 | 0.750000 | 1.050000 | 1.333333 | 1.607150 | 1/4 (n - 4/n) |
| 17 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | |
| 1-14, 2-10, 4-11, 5-13 | 45 | 34 | 30 | 27 | 22 | 18 | 16 | 2/n = tan a |
| 3- 7, 3- 8 | 79 | 73 | 71 | 68 | 63 | 59 | 55 | 10/n = tan b |
| 6-10, 6-14, 9-11, 9-13 | 45 | 56 | 60 | 63 | 68 | 72 | 74 | 90 - a |
| 10-15, 11-12, 12-16 | 90 | 68 | 60 | 54 | 44 | 36 | 32 | 2a |
| 7-15, 8-12 | 34 | 39 | 41 | 41 | 41 | 41 | 39 | b = a |
| 7-10, 8-11 | 56 | 73 | 79 | 85 | 95 | 103 | 109 | 180 - a - b |
| 13-17 | 0 | 22 | 30 | 36 | 46 | 54 | 58 | 90 - 2a |
| 7-8 | 22 | 34 | 38 | 44 | 54 | 62 | 70 | 180 - 2b |
| 1-6, 2-6, 4-9, 5- 9, 16-17 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |

4 PANELS AT TOP & BOTTOM



$$\text{PITCH} = \frac{H}{L} = \frac{1}{n}$$

$$n = \frac{1}{H}$$

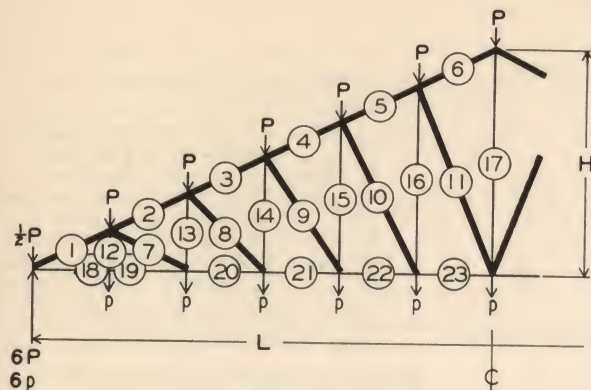
$$N = \sqrt{n^2 + 4}$$

To find the length of any member, multiply the height of truss H by the length coefficient under H .

[illegible]

TRUSSES-STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES-TRIANGULAR HOWE

12 PANELS AT TOP & BOTTOM



$$\text{PITCH} = \frac{H}{L} = \frac{1}{n}$$

$$n = \frac{L}{H}$$

$$N = \sqrt{n^2 + 4}$$

To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

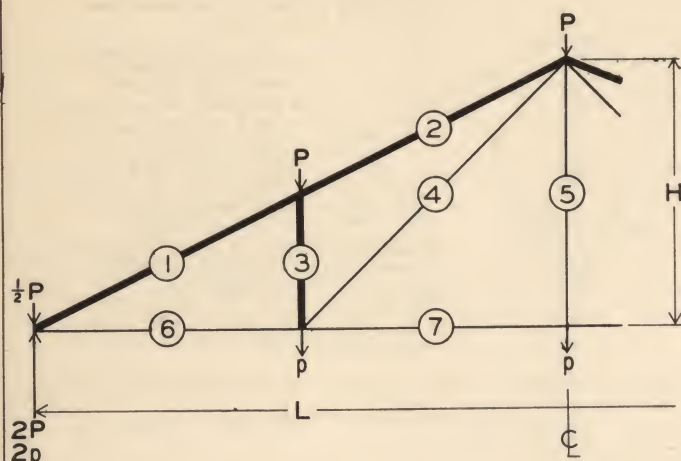
ALL MEMBERS WHICH ARE IN COMPRESSION MUST BE DESIGNED AS COLUMNS

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | | | | | | | | GENERAL FORMULAS | |
|---|-------------|----------|----------|----------|----------|----------|----------|-------------|----------|----------|----------|----------|----------|----------|------------------|-----------------|
| | 2 | 3 | 2√3 | 4 | 5 | 6 | 7 | | | | | | | | | |
| STRESS COEFFICIENTS | | | | | | | | | | | | | | | | |
| | P | p | P | p | P | p | P | p | P | p | P | p | P | p | P | P |
| 1 | -7.78 | -7.78 | -9.92 | -9.92 | -11.00 | -11.00 | -12.30 | -12.30 | -14.81 | -14.81 | -17.39 | -17.39 | -20.02 | -20.02 | - 11/4 N | - 11/4 N |
| 2 | -7.07 | -7.07 | -9.01 | -9.01 | -10.00 | -10.00 | -11.18 | -11.18 | -13.46 | -13.46 | -15.81 | -15.81 | -18.20 | -18.20 | - 5/2 N | - 5/2 N |
| 3 | -6.36 | -6.36 | -8.11 | -8.11 | -9.00 | -9.00 | -10.06 | -10.06 | -12.12 | -12.12 | -14.23 | -14.23 | -16.38 | -16.38 | - 9/4 N | - 9/4 N |
| 4 | -5.66 | -5.66 | -7.21 | -7.21 | -8.00 | -8.00 | -8.94 | -8.94 | -10.77 | -10.77 | -12.65 | -12.65 | -14.56 | -14.56 | - 2 N | - 2 N |
| 5 | -4.96 | -4.96 | -6.31 | -6.31 | -7.00 | -7.00 | -7.83 | -7.83 | -9.42 | -9.42 | -11.07 | -11.07 | -12.74 | -12.74 | - 7/4 N | - 7/4 N |
| 6 | -4.24 | -4.24 | -5.41 | -5.41 | -6.00 | -6.00 | -6.71 | -6.71 | -8.08 | -8.08 | -9.49 | -9.49 | -10.92 | -10.92 | - 3/2 N | - 3/2 N |
| 7 | -0.71 | -0.71 | -0.90 | -0.90 | -1.00 | -1.00 | -1.12 | -1.12 | -1.35 | -1.35 | -1.58 | -1.58 | -1.82 | -1.82 | - 1/4 N | - 1/4 N |
| 8 | -1.12 | -1.12 | -1.25 | -1.25 | -1.32 | -1.32 | -1.41 | -1.41 | -1.60 | -1.60 | -1.80 | -1.80 | -2.02 | -2.02 | - 1/4 √n² + 16 | - 1/4 √n² + 16 |
| 9 | -1.68 | -1.68 | -1.68 | -1.68 | -1.73 | -1.73 | -1.80 | -1.80 | -1.95 | -1.95 | -2.12 | -2.12 | -2.30 | -2.30 | - 1/4 √n² + 36 | - 1/4 √n² + 36 |
| 10 | -2.06 | -2.06 | -2.14 | -2.14 | -2.18 | -2.18 | -2.24 | -2.24 | -2.36 | -2.36 | -2.50 | -2.50 | -2.66 | -2.66 | - 1/4 √n² + 64 | - 1/4 √n² + 64 |
| 11 | -2.66 | -2.66 | -2.61 | -2.61 | -2.65 | -2.65 | -2.69 | -2.69 | -2.80 | -2.80 | -2.92 | -2.92 | -3.05 | -3.05 | - 1/4 √n² + 100 | - 1/4 √n² + 100 |
| 12 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1 |
| 13 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 1/2 | 3/2 |
| 14 | 1.00 | 2.00 | 1.00 | 2.00 | 1.00 | 2.00 | 1.00 | 2.00 | 1.00 | 2.00 | 1.00 | 2.00 | 1.00 | 2.00 | 1 | 2 |
| 15 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 3/2 | 5/2 |
| 16 | 2.00 | 3.00 | 2.00 | 3.00 | 2.00 | 3.00 | 2.00 | 3.00 | 2.00 | 3.00 | 2.00 | 3.00 | 2.00 | 3.00 | 2 | 3 |
| 17 | 5.00 | 6.00 | 5.00 | 6.00 | 5.00 | 6.00 | 5.00 | 6.00 | 5.00 | 6.00 | 5.00 | 6.00 | 5.00 | 6.00 | 5 | 6 |
| 18 | 5.50 | 5.50 | 8.25 | 8.25 | 9.53 | 9.53 | 11.00 | 11.00 | 13.75 | 13.75 | 16.50 | 16.50 | 19.25 | 19.25 | 11/4 n | 11/4 n |
| 19 | 5.50 | 5.50 | 8.25 | 8.25 | 9.53 | 9.53 | 11.00 | 11.00 | 13.75 | 13.75 | 16.50 | 16.50 | 19.25 | 19.25 | 11/4 n | 11/4 n |
| 20 | 5.00 | 5.00 | 7.50 | 7.50 | 8.66 | 8.66 | 10.00 | 10.00 | 12.50 | 12.50 | 15.00 | 15.00 | 17.50 | 17.50 | 5/2 n | 5/2 n |
| 21 | 4.50 | 4.50 | 6.75 | 6.75 | 7.79 | 7.79 | 9.00 | 9.00 | 11.25 | 11.25 | 13.50 | 13.50 | 15.75 | 15.75 | 9/4 n | 9/4 n |
| 22 | 4.00 | 4.00 | 6.00 | 6.00 | 6.93 | 6.93 | 8.00 | 8.00 | 10.00 | 10.00 | 12.00 | 12.00 | 14.00 | 14.00 | 2 n | 2 n |
| 23 | 3.50 | 3.50 | 5.25 | 5.25 | 6.06 | 6.06 | 7.00 | 7.00 | 8.75 | 8.75 | 10.50 | 10.50 | 12.25 | 12.25 | 7/4 n | 7/4 n |
| LENGTH COEFFICIENTS | | | | | | | | | | | | | | | | |
| | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H |
| 1, 2, 3, 4, 5, 6, 7 | 0.235702 | 0.300463 | 0.333333 | 0.372878 | 0.448764 | 0.527046 | 0.606676 | 0.606676 | 0.606676 | 0.606676 | 0.606676 | 0.606676 | 0.606676 | 0.606676 | 0.606676 | 1/12 N |
| 8 | 0.372878 | 0.416667 | 0.440989 | 0.471406 | 0.533594 | 0.600925 | 0.671855 | 0.671855 | 0.671855 | 0.671855 | 0.671855 | 0.671855 | 0.671855 | 0.671855 | 0.671855 | 1/12 √n² + 16 |
| 9 | 0.527046 | 0.569017 | 0.577350 | 0.600925 | 0.650854 | 0.707107 | 0.768295 | 0.768295 | 0.768295 | 0.768295 | 0.768295 | 0.768295 | 0.768295 | 0.768295 | 0.768295 | 1/12 √n² + 36 |
| 10 | 0.607184 | 0.712000 | 0.726483 | 0.745556 | 0.786166 | 0.833333 | 0.885845 | 0.885845 | 0.885845 | 0.885845 | 0.885845 | 0.885845 | 0.885845 | 0.885845 | 0.885845 | 1/12 √n² + 64 |
| 11 | 0.849857 | 0.870026 | 0.881917 | 0.897527 | 0.931696 | 0.971825 | 1.017213 | 1.017213 | 1.017213 | 1.017213 | 1.017213 | 1.017213 | 1.017213 | 1.017213 | 1.017213 | 1/12 √n² + 100 |
| 12 | 0.166667 | 0.166667 | 0.166667 | 0.166667 | 0.166667 | 0.166667 | 0.166667 | 0.166667 | 0.166667 | 0.166667 | 0.166667 | 0.166667 | 0.166667 | 0.166667 | 0.166667 | 1/6 |
| 13 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 1/3 |
| 14 | 0.500000 | 0.500000 | 0.500000 | 0.500000 | 0.500000 | 0.500000 | 0.500000 | 0.500000 | 0.500000 | 0.500000 | 0.500000 | 0.500000 | 0.500000 | 0.500000 | 0.500000 | 1/2 |
| 15 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 2/3 |
| 16 | 0.833333 | 0.833333 | 0.833333 | 0.833333 | 0.833333 | 0.833333 | 0.833333 | 0.833333 | 0.833333 | 0.833333 | 0.833333 | 0.833333 | 0.833333 | 0.833333 | 0.833333 | 5/6 |
| 17 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 |
| 18, 19, 20, 21, 22, 23 | 0.166667 | 0.250000 | 0.288667 | 0.333333 | 0.416667 | 0.500000 | 0.583333 | 0.583333 | 0.583333 | 0.583333 | 0.583333 | 0.583333 | 0.583333 | 0.583333 | 0.583333 | 1/12 n |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | | | | | | | | | |
| 1-18, 7-19 | 45 | 34 | 30 | 27 | 22 | 18 | 16 | 2/n = tan a | | | | | | | | |
| 8-20 | 63 | 53 | 49 | 45 | 39 | 34 | 30 | 4/n = tan b | | | | | | | | |
| 9-21 | 72 | 63 | 60 | 56 | 50 | 45 | 41 | 5/n = tan c | | | | | | | | |
| 10-22 | 76 | 69 | 67 | 63 | 58 | 53 | 49 | 6/n = tan d | | | | | | | | |
| 11-23 | 79 | 73 | 71 | 68 | 63 | 59 | 55 | 7/n = tan e | | | | | | | | |
| 1-12, 2-13, 3-14, 4-15, 5-16, 6-17, 7-18 | 45 | 56 | 60 | 63 | 68 | 72 | 74 | 90 - a | | | | | | | | |
| 8-13, 8-14 | 27 | 37 | 41 | 45 | 51 | 56 | 60 | 90 - b | | | | | | | | |
| 9-14, 9-15 | 18 | 27 | 30 | 34 | 40 | 45 | 49 | 90 - c | | | | | | | | |
| 10-16, 10-16 | 14 | 21 | 23 | 27 | 32 | 37 | 41 | 90 - d | | | | | | | | |
| 11-16, 11-17 | 11 | 17 | 19 | 22 | 27 | 31 | 35 | 90 - e | | | | | | | | |
| 2-7 | 90 | 68 | 60 | 54 | 44 | 36 | 32 | 2a | | | | | | | | |
| 3-8 | 108 | 87 | 79 | 72 | 61 | 52 | 46 | a + b | | | | | | | | |
| 4-9 | 117 | 97 | 90 | 83 | 72 | 63 | 57 | a + c | | | | | | | | |
| 5-10 | 121 | 103 | 97 | 90 | 80 | 71 | 65 | a + d | | | | | | | | |
| 6-11 | 124 | 107 | 101 | 95 | 85 | 77 | 71 | a + e | | | | | | | | |
| 12-18, 12-19, 13-20, 14-21, 14-22, 15-23 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | | | | | | | | |

4 PANELS AT TOP & BOTTOM



$$\text{PITCH} = \frac{H}{L} = \frac{1}{n}$$

$$\eta = \frac{L}{H}$$

$$N = \sqrt{n^2 + 4}$$

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

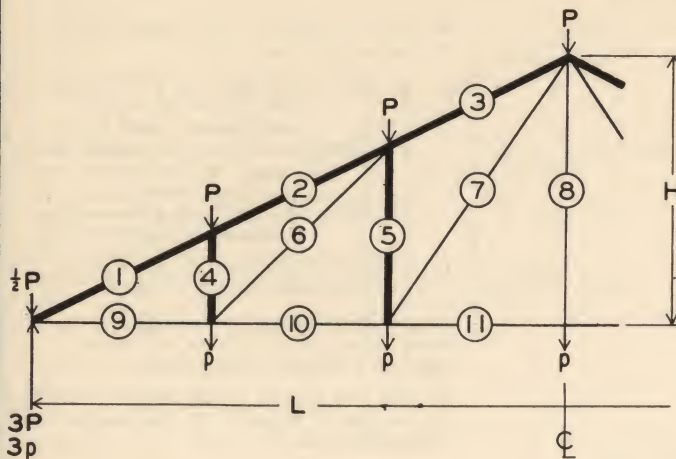
Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

[illegible]

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - TRIANGULAR PRATT

6 PANELS AT TOP & BOTTOM



To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

$$\text{PITCH} = \frac{H}{L} = \frac{1}{n}$$

$$n = \frac{L}{H}$$

$$N = \sqrt{n^2 + 4}$$

ALL MEMBERS WHICH ARE IN COMPRESSION
MUST BE DESIGNED AS COLUMNS

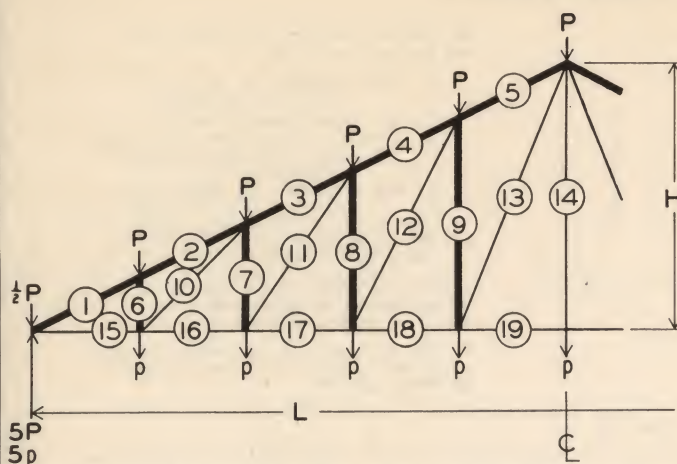
Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | | | | | | | | GENERAL FORMULAS | |
|---|-------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------------------|--------------|
| | 2 | 3 | 2√3 | 4 | 5 | 6 | 7 | | | | | | | | | |
| STRESS COEFFICIENTS | | | | | | | | | | | | | | | | |
| | P | p | P | p | P | p | P | p | P | p | P | p | P | p | P | p |
| 1 | -3.54 | -3.54 | -4.51 | -4.51 | -5.00 | -5.00 | -5.59 | -5.59 | -6.73 | -6.73 | -7.91 | -7.91 | -9.10 | -9.10 | - 5/4 N | - 5/4 N |
| 2 | -3.54 | -3.54 | -4.51 | -4.51 | -5.00 | -5.00 | -5.59 | -5.59 | -6.73 | -6.73 | -7.91 | -7.91 | -9.10 | -9.10 | - 5/4 N | - 5/4 N |
| 3 | -2.83 | -2.83 | -3.61 | -3.61 | -4.00 | -4.00 | -4.47 | -4.47 | -5.39 | -5.39 | -6.32 | -6.32 | -7.28 | -7.28 | - N | - N |
| 4 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | - 1 | 0 |
| 5 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | - 3/2 | - 1/2 |
| 6 | 1.12 | 1.12 | 1.25 | 1.25 | 1.32 | 1.32 | 1.41 | 1.41 | 1.60 | 1.60 | 1.80 | 1.80 | 2.02 | 2.02 | 1/4 √n² + 16 | 1/4 √n² + 16 |
| 7 | 1.58 | 1.58 | 1.68 | 1.68 | 1.73 | 1.73 | 1.80 | 1.80 | 1.95 | 1.95 | 2.12 | 2.12 | 2.30 | 2.30 | 1/4 √n² + 36 | 1/4 √n² + 36 |
| 8 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1 |
| 9 | 2.50 | 2.50 | 3.75 | 3.75 | 4.33 | 4.33 | 5.00 | 5.00 | 6.25 | 6.25 | 7.50 | 7.50 | 8.75 | 8.75 | 5/4 n | 5/4 n |
| 10 | 2.00 | 2.00 | 3.00 | 3.00 | 3.46 | 3.46 | 4.00 | 4.00 | 5.00 | 5.00 | 6.00 | 6.00 | 7.00 | 7.00 | n | n |
| 11 | 1.50 | 1.50 | 2.25 | 2.25 | 2.60 | 2.60 | 3.00 | 3.00 | 3.75 | 3.75 | 4.50 | 4.50 | 5.25 | 5.25 | 3/4 n | 3/4 n |
| LENGTH COEFFICIENTS | | | | | | | | | | | | | | | | |
| | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H |
| 1, 2, 3 | 0.471405 | 0.600925 | 0.666075 | 0.745356 | 0.897527 | 1.054093 | 1.213352 | 1.383333 | 1.554093 | 1.725352 | 1.897527 | 2.072527 | 2.249093 | 2.426352 | 2.604093 | 1/6 N |
| 4 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 0.333333 | 1/3 |
| 5 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 0.666667 | 2/3 |
| 6 | 0.745356 | 0.833333 | 0.881917 | 0.942809 | 1.067187 | 1.201850 | 1.343710 | 1.492809 | 1.648187 | 1.809187 | 1.975810 | 2.148187 | 2.326352 | 2.509093 | 2.696352 | 1/6 √n² + 16 |
| 7 | 1.054093 | 1.118034 | 1.154701 | 1.201850 | 1.301708 | 1.412214 | 1.533691 | 1.666093 | 1.809187 | 1.961850 | 2.124093 | 2.295810 | 2.477093 | 2.667810 | 2.868093 | 1/6 √n² + 36 |
| 8 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 |
| 9, 10, 11 | 0.333333 | 0.500000 | 0.577333 | 0.666667 | 0.833333 | 1.000000 | 1.166667 | 1.333333 | 1.500000 | 1.666667 | 1.833333 | 2.000000 | 2.166667 | 2.333333 | 2.500000 | 1/6 n |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | | | | | | | | | |
| 1- 9 | 45 | 34 | 30 | 27 | 22 | 18 | 16 | 14 | 12 | 10 | 8 | 6 | 4 | 2 | 1 | 2/n = tan a |
| 8-10 | 53 | 53 | 49 | 45 | 39 | 34 | 30 | 26 | 22 | 18 | 14 | 10 | 6 | 2 | 1 | 4/n = tan b |
| 7-11 | 72 | 63 | 60 | 56 | 50 | 45 | 41 | 36 | 32 | 28 | 24 | 20 | 16 | 12 | 8 | 6/n = tan c |
| 1- 4 | 45 | 56 | 60 | 63 | 68 | 72 | 74 | 76 | 78 | 80 | 82 | 84 | 86 | 88 | 90 | 90 - a |
| 4-6, 5-6 | 27 | 37 | 41 | 45 | 51 | 56 | 60 | 64 | 68 | 72 | 76 | 80 | 84 | 88 | 90 | 90 - b |
| 5-7, 7-8 | 18 | 27 | 30 | 34 | 40 | 45 | 49 | 53 | 57 | 61 | 65 | 69 | 73 | 77 | 81 | 90 - c |
| 2- 6 | 18 | 19 | 19 | 18 | 17 | 16 | 14 | 12 | 10 | 8 | 6 | 4 | 2 | 1 | 1 | b - a |
| 3- 7 | 27 | 29 | 30 | 29 | 28 | 27 | 25 | 23 | 21 | 19 | 17 | 15 | 13 | 11 | 9 | c - a |
| 2-4, 3-5 | 135 | 124 | 120 | 117 | 112 | 108 | 106 | 104 | 102 | 100 | 98 | 96 | 94 | 92 | 90 | 90 + a |
| 4-9, 5-10, 8-11 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - TRIANGULAR PRATT

10 PANELS AT TOP & BOTTOM



To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

$$\text{PITCH} = \frac{H}{L} = \frac{1}{n}$$

$$n = \frac{L}{H}$$

$$N = \sqrt{n^2 + 4}$$

ALL MEMBERS WHICH ARE IN COMPRESSION
MUST BE DESIGNED AS COLUMNS

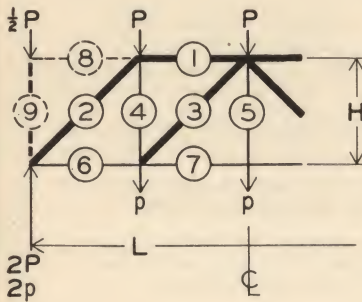
Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | | | | | | | | GENERAL FORMULAS | |
|---|-------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------------------|----------------|
| | 2 | 3 | 2√3 | 4 | 5 | 6 | 7 | | | | | | | | | |
| STRESS COEFFICIENTS | | | | | | | | | | | | | | | | |
| | P | p | P | p | P | p | P | p | P | p | P | p | P | p | P | p |
| 1 | -6.36 | -6.36 | -8.11 | -8.11 | -9.00 | -9.00 | -10.06 | -10.06 | -12.12 | -12.12 | -14.23 | -14.23 | -16.38 | -16.38 | - 9/4 N | - 9/4 N |
| 2 | -6.36 | -6.36 | -8.11 | -8.11 | -9.00 | -9.00 | -10.06 | -10.06 | -12.12 | -12.12 | -14.23 | -14.23 | -16.38 | -16.38 | - 9/4 N | - 9/4 N |
| 3 | -5.66 | -5.66 | -7.21 | -7.21 | -8.00 | -8.00 | - 8.94 | - 8.94 | -10.77 | -10.77 | -12.65 | -12.65 | -14.56 | -14.56 | - 2 N | - 2 N |
| 4 | -4.95 | -4.95 | -6.31 | -6.31 | -7.00 | -7.00 | - 7.83 | - 7.83 | - 9.42 | - 9.42 | -11.07 | -11.07 | -12.74 | -12.74 | - 7/4 N | - 7/4 N |
| 5 | -4.24 | -4.24 | -5.41 | -5.41 | -6.00 | -6.00 | - 6.71 | - 6.71 | - 8.08 | - 8.08 | - 9.49 | - 9.49 | -10.92 | -10.92 | - 3/2 N | - 3/2 N |
| 6 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1 | 0 |
| 7 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | - 1.50 | -0.50 | - 1.50 | -0.50 | - 1.50 | -0.50 | - 1.50 | -0.50 | - 3/2 | - 1/2 |
| 8 | -2.00 | -1.00 | -2.00 | -1.00 | -2.00 | -1.00 | - 2.00 | - 1.00 | - 2.00 | - 1.00 | - 2.00 | - 1.00 | - 2.00 | - 1.00 | - 2 | - 1 |
| 9 | -2.50 | -1.50 | -2.50 | -1.50 | -2.50 | -1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 5/2 | - 3/2 |
| 10 | 1.12 | 1.12 | 1.25 | 1.25 | 1.32 | 1.32 | 1.41 | 1.41 | 1.60 | 1.60 | 1.80 | 1.80 | 2.02 | 2.02 | 1/4 √n² + 16 | 1/4 √n² + 16 |
| 11 | 1.58 | 1.58 | 1.68 | 1.68 | 1.73 | 1.73 | 1.80 | 1.80 | 1.95 | 1.95 | 2.12 | 2.12 | 2.30 | 2.30 | 1/4 √n² + 36 | 1/4 √n² + 33 |
| 12 | 2.06 | 2.06 | 2.14 | 2.14 | 2.18 | 2.18 | 2.24 | 2.24 | 2.36 | 2.36 | 2.50 | 2.50 | 2.66 | 2.66 | 1/4 √n² + 64 | 1/4 √n² + 64 |
| 13 | 2.55 | 2.55 | 2.61 | 2.61 | 2.65 | 2.65 | 2.69 | 2.69 | 2.80 | 2.80 | 2.92 | 2.92 | 3.05 | 3.05 | 1/4 √n² + 100 | 1/4 √n² + 100 |
| 14 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1 |
| 15 | 4.50 | 4.50 | 6.75 | 6.75 | 7.79 | 7.79 | 9.00 | 9.00 | 11.25 | 11.25 | 13.50 | 13.50 | 15.75 | 15.75 | 9/4 n | 9/4 n |
| 16 | 4.00 | 4.00 | 6.00 | 6.00 | 6.93 | 6.93 | 8.00 | 8.00 | 10.00 | 10.00 | 12.00 | 12.00 | 14.00 | 14.00 | 2 n | 2 n |
| 17 | 3.50 | 3.50 | 5.25 | 5.25 | 6.06 | 6.06 | 7.00 | 7.00 | 8.75 | 8.75 | 10.50 | 10.50 | 12.25 | 12.25 | 7/4 n | 7/4 n |
| 18 | 3.00 | 3.00 | 4.50 | 4.50 | 5.20 | 5.20 | 6.00 | 6.00 | 7.50 | 7.50 | 9.00 | 9.00 | 10.50 | 10.50 | 3/2 n | 3/2 n |
| 19 | 2.50 | 2.50 | 3.75 | 3.75 | 4.33 | 4.33 | 5.00 | 5.00 | 6.25 | 6.25 | 7.50 | 7.50 | 8.75 | 8.75 | 5/4 n | 5/4 n |
| LENGTH COEFFICIENTS | | | | | | | | | | | | | | | | |
| | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H |
| 1, 2, 3, 4, 5 | 0.282843 | 0.360555 | 0.400000 | 0.447214 | 0.538516 | 0.632456 | 0.728011 | 0.824566 | 0.921964 | 1.020000 | 1.118034 | 1.216619 | 1.315656 | 1.415136 | 1.515056 | 1/10 N |
| 6 | 0.200000 | 0.200000 | 0.200000 | 0.200000 | 0.200000 | 0.200000 | 0.200000 | 0.200000 | 0.200000 | 0.200000 | 0.200000 | 0.200000 | 0.200000 | 0.200000 | 0.200000 | 1/5 |
| 7 | 0.400000 | 0.400000 | 0.400000 | 0.400000 | 0.400000 | 0.400000 | 0.400000 | 0.400000 | 0.400000 | 0.400000 | 0.400000 | 0.400000 | 0.400000 | 0.400000 | 0.400000 | 2/5 |
| 8 | 0.600000 | 0.600000 | 0.600000 | 0.600000 | 0.600000 | 0.600000 | 0.600000 | 0.600000 | 0.600000 | 0.600000 | 0.600000 | 0.600000 | 0.600000 | 0.600000 | 0.600000 | 3/5 |
| 9 | 0.800000 | 0.800000 | 0.800000 | 0.800000 | 0.800000 | 0.800000 | 0.800000 | 0.800000 | 0.800000 | 0.800000 | 0.800000 | 0.800000 | 0.800000 | 0.800000 | 0.800000 | 4/5 |
| 10 | 0.447214 | 0.500000 | 0.529150 | 0.565685 | 0.640312 | 0.721110 | 0.81025 | 0.943398 | 1.000000 | 1.063015 | 1.220656 | 1.415136 | 1.661190 | 1.961190 | 2.315656 | 1/10 √n² + 16 |
| 11 | 0.632456 | 0.670820 | 0.692820 | 0.721110 | 0.781025 | 0.846528 | 0.921964 | 1.000000 | 1.063015 | 1.220656 | 1.415136 | 1.661190 | 1.961190 | 2.315656 | 2.815656 | 1/10 √n² + 36 |
| 12 | 0.824566 | 0.854400 | 0.871780 | 0.894427 | 0.943398 | 1.000000 | 1.063015 | 1.220656 | 1.415136 | 1.661190 | 1.961190 | 2.315656 | 2.815656 | 3.415656 | 4.015656 | 1/10 √n² + 64 |
| 13 | 1.019804 | 1.044031 | 1.058301 | 1.077033 | 1.118034 | 1.166190 | 1.220656 | 1.415136 | 1.661190 | 1.961190 | 2.315656 | 2.815656 | 3.415656 | 4.015656 | 4.615656 | 1/10 √n² + 100 |
| 14 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 |
| 15, 16, 17, 18, 19 | 0.200000 | 0.300000 | 0.346400 | 0.400000 | 0.500000 | 0.600000 | 0.700000 | 0.800000 | 0.900000 | 1.000000 | 1.100000 | 1.200000 | 1.300000 | 1.400000 | 1.500000 | 1/10 n |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | | | | | | | | | |
| 1-15 | 45 | 34 | 30 | 27 | 22 | 18 | 16 | 14 | 12 | 10 | 8 | 6 | 4 | 2 | 0 | 2/n = tan a |
| 10-16 | 63 | 53 | 49 | 45 | 39 | 34 | 30 | 26 | 22 | 18 | 14 | 10 | 6 | 2 | 0 | 4/n = tan b |
| 11-17 | 72 | 63 | 60 | 56 | 50 | 45 | 41 | 36 | 32 | 26 | 22 | 18 | 14 | 10 | 6 | 6/n = tan c |
| 12-18 | 76 | 69 | 67 | 63 | 58 | 53 | 49 | 44 | 40 | 34 | 30 | 26 | 22 | 18 | 14 | 8/n = tan d |
| 13-19 | 79 | 73 | 71 | 68 | 64 | 59 | 55 | 50 | 46 | 40 | 36 | 32 | 28 | 24 | 20 | 10/n = tan e |
| 1- 6 | 45 | 56 | 60 | 63 | 68 | 72 | 74 | 76 | 78 | 80 | 82 | 84 | 86 | 88 | 90 | 90 - a |
| 6-10, 7-10 | 27 | 37 | 41 | 45 | 51 | 56 | 60 | 64 | 68 | 72 | 76 | 80 | 84 | 88 | 90 | 90 - b |
| 7-11, 8-11 | 18 | 27 | 30 | 34 | 40 | 45 | 49 | 53 | 58 | 63 | 68 | 72 | 76 | 80 | 84 | 90 - c |
| 8-12, 9-12 | 14 | 21 | 23 | 27 | 32 | 37 | 41 | 46 | 50 | 55 | 60 | 64 | 68 | 72 | 76 | 90 - d |
| 9-13, 13-14 | 11 | 17 | 19 | 22 | 26 | 31 | 35 | 40 | 44 | 49 | 54 | 58 | 63 | 68 | 72 | 90 - e |
| 2-10 | 18 | 19 | 19 | 18 | 17 | 16 | 14 | 12 | 10 | 8 | 6 | 4 | 2 | 0 | 0 | b - a |
| 3-11 | 27 | 29 | 30 | 29 | 28 | 27 | 25 | 23 | 21 | 19 | 17 | 14 | 12 | 10 | 8 | c - a |
| 4-12 | 31 | 35 | 37 | 36 | 35 | 33 | 31 | 29 | 27 | 25 | 23 | 21 | 19 | 17 | 14 | d - a |
| 5-13 | 34 | 39 | 41 | 41 | 42 | 41 | 39 | 37 | 35 | 33 | 31 | 29 | 27 | 25 | 23 | e - a |
| 2-6, 3-7, 4-8, 5-9 | 135 | 124 | 120 | 117 | 112 | 108 | 106 | 104 | 102 | 100 | 98 | 96 | 94 | 92 | 90 | 90 + a |
| 6-15, 7-16, 8-17, 9-18, 14-19 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - FLAT HOWE

4 PANELS AT TOP & BOTTOM



$$n = \frac{L}{H}$$

$$N \equiv \sqrt{n^2 + 16}$$

To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

ALL MEMBERS WHICH ARE IN COMPRESSION
MUST BE DESIGNED AS COLUMNS

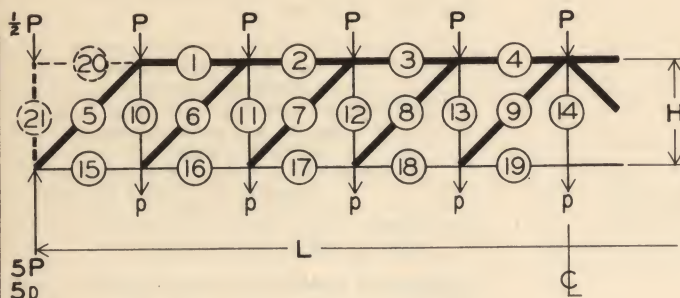
Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

[illegible]

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - FLAT HOWE

10 PANELS AT TOP & BOTTOM



$$n = \frac{L}{H}$$

$$N = \sqrt{n^2 + 100}$$

To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

ALL MEMBERS WHICH ARE IN COMPRESSION MUST BE DESIGNED AS COLUMNS

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | | | | | | | | GENERAL FORMULAS | |
|---------------------|-------------|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------------------|-----------|
| | 7 | 8 | | 9 | | 10 | | 11 | | 12 | | 13 | | | | |
| STRESS COEFFICIENTS | | | | | | | | | | | | | | | | |
| | P | p | P | p | P | p | P | p | P | p | P | p | P | p | P | p |
| 1 | -3.15 | -3.15 | -3.60 | -3.60 | -4.05 | -4.05 | -4.50 | -4.50 | -4.95 | -4.95 | -5.40 | -5.40 | -5.85 | -5.85 | - 9/20 n | - 9/20 n |
| 2 | -5.60 | -5.60 | -6.40 | -6.40 | -7.20 | -7.20 | -8.00 | -8.00 | -8.80 | -8.80 | -9.60 | -9.60 | -10.40 | -10.40 | - 4/5 n | - 4/5 n |
| 3 | -7.35 | -7.35 | -8.40 | -8.40 | -9.45 | -9.45 | -10.50 | -10.50 | -11.55 | -11.55 | -12.60 | -12.60 | -13.65 | -13.65 | - 21/20 n | - 21/20 n |
| 4 | -8.40 | -8.40 | -9.60 | -9.60 | -10.80 | -10.80 | -12.00 | -12.00 | -13.20 | -13.20 | -14.40 | -14.40 | -15.60 | -15.60 | - 6/5 n | - 6/5 n |
| 5 | -5.49 | -5.49 | -5.76 | -5.76 | -6.05 | -6.05 | -6.36 | -6.36 | -6.69 | -6.69 | -7.03 | -7.03 | -7.38 | -7.38 | - 9/20 N | - 9/20 N |
| 6 | -4.27 | -4.27 | -4.48 | -4.48 | -4.71 | -4.71 | -4.95 | -4.95 | -5.20 | -5.20 | -5.47 | -5.47 | -5.74 | -5.74 | - 7/20 N | - 7/20 N |
| 7 | -3.05 | -3.05 | -3.20 | -3.20 | -3.36 | -3.36 | -3.64 | -3.64 | -3.72 | -3.72 | -3.91 | -3.91 | -4.10 | -4.10 | - 1/4 N | - 1/4 N |
| 8 | -1.83 | -1.83 | -1.92 | -1.92 | -2.02 | -2.02 | -2.12 | -2.12 | -2.23 | -2.23 | -2.34 | -2.34 | -2.46 | -2.46 | - 3/20 N | - 3/20 N |
| 9 | -0.61 | -0.61 | -0.64 | -0.64 | -0.67 | -0.67 | -0.71 | -0.71 | -0.74 | -0.74 | -0.78 | -0.78 | -0.82 | -0.82 | - 1/20 N | - 1/20 N |
| 10 | 3.50 | 4.50 | 3.50 | 4.50 | 3.50 | 4.50 | 3.50 | 4.50 | 3.50 | 4.50 | 3.50 | 4.50 | 3.50 | 4.50 | 7/2 | 9/2 |
| 11 | 2.50 | 3.50 | 2.50 | 3.50 | 2.50 | 3.50 | 2.50 | 3.50 | 2.50 | 3.50 | 2.50 | 3.50 | 2.50 | 3.50 | 5/2 | 7/2 |
| 12 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 3/2 | 5/2 |
| 13 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 1/2 | 3/2 |
| 14 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1 |
| 15 | 3.15 | 3.15 | 3.60 | 3.60 | 4.05 | 4.05 | 4.50 | 4.50 | 4.95 | 4.95 | 5.40 | 5.40 | 5.85 | 5.85 | 9/20 n | 9/20 n |
| 16 | 5.60 | 5.60 | 6.40 | 6.40 | 7.20 | 7.20 | 8.00 | 8.00 | 8.80 | 8.80 | 9.60 | 9.60 | 10.40 | 10.40 | 4/5 n | 4/5 n |
| 17 | 7.35 | 7.35 | 8.40 | 8.40 | 9.45 | 9.45 | 10.50 | 10.50 | 11.55 | 11.55 | 12.60 | 12.60 | 13.65 | 13.65 | 21/20 n | 21/20 n |
| 18 | 8.40 | 8.40 | 9.60 | 9.60 | 10.80 | 10.80 | 12.00 | 12.00 | 13.20 | 13.20 | 14.40 | 14.40 | 15.60 | 15.60 | 6/5 n | 6/5 n |
| 19 | 8.75 | 8.75 | 10.00 | 10.00 | 11.25 | 11.25 | 12.50 | 12.50 | 13.75 | 13.75 | 15.00 | 15.00 | 16.25 | 16.25 | 5/4 n | 5/4 n |
| 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21 | -0.50 | 0 | -0.50 | 0 | -0.50 | 0 | -0.50 | 0 | -0.50 | 0 | -0.50 | 0 | -0.50 | 0 | - 1/2 | 0 |

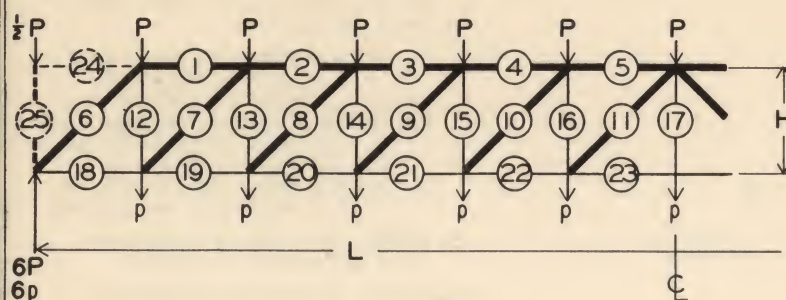
LENGTH COEFFICIENTS

| | H | H | H | H | H | H | H | H |
|------------|----------|----------|----------|----------|----------|----------|----------|--------|
| Horizontal | 0.700000 | 0.800000 | 0.900000 | 1.000000 | 1.100000 | 1.200000 | 1.300000 | 1/10 n |
| Diagonal | 1.220656 | 1.280625 | 1.345362 | 1.414214 | 1.486607 | 1.562050 | 1.640122 | 1/10 N |
| Vertical | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 |

ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS

| | | | | | | | | |
|---|----|----|----|----|----|----|----|--------------|
| Between diagonal and horizontal members | 55 | 51 | 48 | 45 | 42 | 40 | 38 | 10/n = tan a |
| Between diagonal and vertical members | 35 | 39 | 42 | 45 | 48 | 50 | 52 | 90 - a |
| Between vertical and horizontal members | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |

12 PANELS AT TOP & BOTTOM



$$n = \frac{1}{H}$$

$$N = \sqrt{n^2 + 144}$$

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | | | | | | | | GENERAL FORMULAS | |
|---|-------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------------------|-----------|
| | 7 | 8 | 9 | 10 | 11 | 12 | 13 | | | | | | | | | |
| STRESS COEFFICIENTS | | | | | | | | | | | | | | | | |
| | P | p | P | p | P | p | P | p | P | p | P | p | P | p | P | p |
| 1 | - 3.21 | - 3.21 | - 3.67 | - 3.67 | - 4.13 | - 4.13 | - 4.58 | - 4.58 | - 5.04 | - 5.04 | - 5.50 | - 5.50 | - 5.96 | - 5.96 | - 11/24 n | - 11/24 n |
| 2 | - 5.83 | - 5.83 | - 6.67 | - 6.67 | - 7.50 | - 7.50 | - 8.33 | - 8.33 | - 9.17 | - 9.17 | - 10.00 | - 10.00 | - 10.83 | - 10.83 | - 5/6 n | - 5/6 n |
| 3 | - 7.88 | - 7.88 | - 9.00 | - 9.00 | - 10.13 | - 10.13 | - 11.25 | - 11.25 | - 12.38 | - 12.38 | - 13.50 | - 13.50 | - 14.63 | - 14.63 | - 9/8 n | - 9/8 n |
| 4 | - 9.33 | - 9.33 | - 10.67 | - 10.67 | - 12.00 | - 12.00 | - 13.33 | - 13.33 | - 14.67 | - 14.67 | - 16.00 | - 16.00 | - 17.33 | - 17.33 | - 4/3 n | - 4/3 n |
| 5 | - 10.21 | - 10.21 | - 11.67 | - 11.67 | - 13.13 | - 13.13 | - 14.58 | - 14.58 | - 16.04 | - 16.04 | - 17.50 | - 17.50 | - 18.96 | - 18.96 | - 35/24 n | - 35/24 n |
| 6 | - 6.37 | - 6.37 | - 6.61 | - 6.61 | - 6.88 | - 6.88 | - 7.16 | - 7.16 | - 7.46 | - 7.46 | - 7.78 | - 7.78 | - 8.11 | - 8.11 | - 11/24 N | - 11/24 N |
| 7 | - 5.21 | - 5.21 | - 5.41 | - 5.41 | - 5.63 | - 5.63 | - 5.86 | - 5.86 | - 6.10 | - 6.10 | - 6.36 | - 6.36 | - 6.63 | - 6.63 | - 3/8 N | - 3/8 N |
| 8 | - 4.06 | - 4.06 | - 4.21 | - 4.21 | - 4.38 | - 4.38 | - 4.56 | - 4.56 | - 4.75 | - 4.75 | - 4.95 | - 4.95 | - 5.16 | - 5.16 | - 7/24 N | - 7/24 N |
| 9 | - 2.89 | - 2.89 | - 3.00 | - 3.00 | - 3.13 | - 3.13 | - 3.25 | - 3.25 | - 3.39 | - 3.39 | - 3.54 | - 3.54 | - 3.69 | - 3.69 | - 5/24 N | - 5/24 N |
| 10 | - 1.74 | - 1.74 | - 1.80 | - 1.80 | - 1.88 | - 1.88 | - 1.95 | - 1.95 | - 2.03 | - 2.03 | - 2.12 | - 2.12 | - 2.21 | - 2.21 | - 1/8 N | - 1/8 N |
| 11 | - 0.58 | - 0.58 | - 0.60 | - 0.60 | - 0.63 | - 0.63 | - 0.65 | - 0.65 | - 0.68 | - 0.68 | - 0.71 | - 0.71 | - 0.74 | - 0.74 | - 1/24 N | - 1/24 N |
| 12 | 4.50 | 5.50 | 4.50 | 5.50 | 4.50 | 5.50 | 4.50 | 5.50 | 4.50 | 5.50 | 4.50 | 5.50 | 4.50 | 5.50 | 9/2 | 11/2 |
| 13 | 3.50 | 4.50 | 3.50 | 4.50 | 3.50 | 4.50 | 3.50 | 4.50 | 3.50 | 4.50 | 3.50 | 4.50 | 3.50 | 4.50 | 7/2 | 9/2 |
| 14 | 2.50 | 3.50 | 2.50 | 3.50 | 2.50 | 3.50 | 2.50 | 3.50 | 2.50 | 3.50 | 2.50 | 3.50 | 2.50 | 3.50 | 5/2 | 7/2 |
| 15 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 1.50 | 2.50 | 3/2 | 5/2 |
| 16 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 0.50 | 1.50 | 1/2 | 3/2 |
| 17 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1 |
| 18 | 3.21 | 3.21 | 3.67 | 3.67 | 4.13 | 4.13 | 4.58 | 4.58 | 5.04 | 5.04 | 5.50 | 5.50 | 5.96 | 5.96 | 11/24 n | 11/24 n |
| 19 | 5.83 | 5.83 | 6.67 | 6.67 | 7.50 | 7.50 | 8.33 | 8.33 | 9.17 | 9.17 | 10.00 | 10.00 | 10.83 | 10.83 | 5/6 n | 5/6 n |
| 20 | 7.88 | 7.88 | 9.00 | 9.00 | 10.13 | 10.13 | 11.25 | 11.25 | 12.38 | 12.38 | 13.50 | 13.50 | 14.63 | 14.63 | 9/8 n | 9/8 n |
| 21 | 9.33 | 9.33 | 10.67 | 10.67 | 12.00 | 12.00 | 13.33 | 13.33 | 14.67 | 14.67 | 16.00 | 16.00 | 17.33 | 17.33 | 4/3 n | 4/3 n |
| 22 | 10.21 | 10.21 | 11.67 | 11.67 | 13.13 | 13.13 | 14.58 | 14.58 | 16.04 | 16.04 | 17.50 | 17.50 | 18.96 | 18.96 | 35/24 n | 35/24 n |
| 23 | 10.50 | 10.50 | 12.00 | 12.00 | 13.50 | 13.50 | 15.00 | 15.00 | 16.50 | 16.50 | 18.00 | 18.00 | 19.50 | 19.50 | 3/2 n | 3/2 n |
| 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 25 | - 0.50 | 0 | - 0.50 | 0 | - 0.50 | 0 | - 0.50 | 0 | - 0.50 | 0 | - 0.50 | 0 | - 0.50 | 0 | - 1/2 | 0 |
| LENGTH COEFFICIENTS | | | | | | | | | | | | | | | | |
| | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H |
| Horizontal | 0.583333 | 0.686667 | 0.750000 | 0.833333 | 0.916667 | 1.000000 | 1.083333 | 1.166667 | 1.250000 | 1.333333 | 1.416667 | 1.500000 | 1.583333 | 1.666667 | 1.750000 | 1.833333 |
| Diagonal | 1.157704 | 1.201850 | 1.250000 | 1.301708 | 1.356568 | 1.414214 | 1.474317 | 1.536864 | 1.601864 | 1.669317 | 1.739224 | 1.811584 | 1.886397 | 1.963664 | 2.043384 | 2.125557 |
| Vertical | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | | | | | | | | | |
| Between diagonal and horizontal members | 60 | 56 | 53 | 50 | 47 | 45 | 43 | 41 | 39 | 37 | 35 | 33 | 31 | 29 | 27 | 25 |
| Between diagonal and vertical members | 30 | 34 | 37 | 40 | 43 | 45 | 47 | 49 | 51 | 53 | 55 | 57 | 59 | 61 | 63 | 65 |
| Between vertical and horizontal members | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |

6 PANELS AT TOP & BOTTOM



$$N = \sqrt{n^2 + 36}$$

To find the length of any member, multiply the height of truss H by the length coefficient under H .

[illegible]

10 PANELS AT TOP & BOTTOM



$$N = \sqrt{n^2 + 100}$$

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | | | | | | | | GENERAL FORMULAS | |
|---|-------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------------------|--------------|
| | 7 | 8 | 9 | 10 | 11 | 12 | 13 | | | | | | | | | |
| STRESS COEFFICIENTS | | | | | | | | | | | | | | | | |
| | P | p | P | p | P | p | P | p | P | p | P | p | P | p | P | p |
| 1 | -3.15 | -3.15 | -3.60 | -3.60 | -4.05 | -4.05 | -4.50 | -4.50 | -4.95 | -4.95 | -5.40 | -5.40 | -5.85 | -5.85 | - 9/20 n | - 9/20 n |
| 2 | -5.60 | -5.60 | -6.40 | -6.40 | -7.20 | -7.20 | -8.00 | -8.00 | -8.80 | -8.80 | -9.60 | -9.60 | -10.40 | -10.40 | - 16/20 n | - 16/20 n |
| 3 | -7.35 | -7.35 | -8.40 | -8.40 | -9.45 | -9.45 | -10.50 | -10.50 | -11.55 | -11.55 | -12.60 | -12.60 | -13.65 | -13.65 | - 21/20 n | - 21/20 n |
| 4 | -8.40 | -8.40 | -9.60 | -9.60 | -10.80 | -10.80 | -12.00 | -12.00 | -13.20 | -13.20 | -14.40 | -14.40 | -15.60 | -15.60 | - 24/20 n | - 24/20 n |
| 5 | -8.75 | -8.75 | -10.00 | -10.00 | -11.25 | -11.25 | -12.50 | -12.50 | -13.75 | -13.75 | -15.00 | -15.00 | -16.25 | -16.25 | - 25/20 n | - 25/20 n |
| 6 | -4.50 | -3.50 | -4.50 | -3.50 | -4.50 | -3.50 | -4.50 | -3.50 | -4.50 | -3.50 | -4.50 | -3.50 | -4.50 | -3.50 | - 9/2 | - 7/2 |
| 7 | -3.50 | -2.50 | -3.50 | -2.50 | -3.50 | -2.50 | -3.50 | -2.50 | -3.50 | -2.50 | -3.50 | -2.50 | -3.50 | -2.50 | - 7/2 | - 5/2 |
| 8 | -2.50 | -1.50 | -2.50 | -1.50 | -2.50 | -1.50 | -2.50 | -1.50 | -2.50 | -1.50 | -2.50 | -1.50 | -2.50 | -1.50 | - 5/2 | - 3/2 |
| 9 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | - 3/2 | - 1/2 |
| 10 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | - 1 | 0 |
| 11 | 5.49 | 5.49 | 5.76 | 5.76 | 6.05 | 6.05 | 6.36 | 6.36 | 6.69 | 6.69 | 7.03 | 7.03 | 7.38 | 7.38 | 9/20 N | 9/20 N |
| 12 | 4.27 | 4.27 | 4.48 | 4.48 | 4.71 | 4.71 | 4.95 | 4.95 | 5.20 | 5.20 | 5.47 | 5.47 | 5.74 | 5.74 | 7/20 N | 7/20 N |
| 13 | 3.05 | 3.05 | 3.20 | 3.20 | 3.36 | 3.36 | 3.54 | 3.54 | 3.72 | 3.72 | 3.91 | 3.91 | 4.10 | 4.10 | 5/20 N | 5/20 N |
| 14 | 1.83 | 1.83 | 1.92 | 1.92 | 2.02 | 2.02 | 2.12 | 2.12 | 2.23 | 2.23 | 2.34 | 2.34 | 2.46 | 2.46 | 3/20 N | 3/20 N |
| 15 | 0.61 | 0.61 | 0.64 | 0.64 | 0.67 | 0.67 | 0.71 | 0.71 | 0.74 | 0.74 | 0.78 | 0.78 | 0.82 | 0.82 | 1/20 N | 1/20 N |
| 16 | 3.15 | 3.15 | 3.60 | 3.60 | 4.05 | 4.05 | 4.50 | 4.50 | 4.95 | 4.95 | 5.40 | 5.40 | 5.85 | 5.85 | 9/20 n | 9/20 n |
| 17 | 5.60 | 5.60 | 6.40 | 6.40 | 7.20 | 7.20 | 8.00 | 8.00 | 8.80 | 8.80 | 9.60 | 9.60 | 10.40 | 10.40 | 16/20 n | 16/20 n |
| 18 | 7.35 | 7.35 | 8.40 | 8.40 | 9.45 | 9.45 | 10.50 | 10.50 | 11.55 | 11.55 | 12.60 | 12.60 | 13.65 | 13.65 | 21/20 n | 21/20 n |
| 19 | 8.40 | 8.40 | 9.60 | 9.60 | 10.80 | 10.80 | 12.00 | 12.00 | 13.20 | 13.20 | 14.40 | 14.40 | 15.60 | 15.60 | 24/20 n | 24/20 n |
| 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21 | -5.00 | 0 | -5.00 | 0 | -5.00 | 0 | -5.00 | 0 | -5.00 | 0 | -5.00 | 0 | -5.00 | 0 | - 5 | 0 |
| LENGTH COEFFICIENTS | | | | | | | | | | | | | | | | |
| | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H |
| Horizontal | 0.700000 | 0.800000 | 0.900000 | 1.000000 | 1.000000 | 1.100000 | 1.200000 | 1.300000 | 1.400000 | 1.500000 | 1.600000 | 1.700000 | 1.800000 | 1.900000 | 2.000000 | 1/10 n |
| Diagonal | 1.220656 | 1.280625 | 1.345362 | 1.414214 | 1.486607 | 1.562050 | 1.640122 | 1.720722 | 1.803850 | 1.889500 | 1.977670 | 2.068360 | 2.161570 | 2.257300 | 2.355550 | 1/10 N |
| Vertical | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | | | | | | | | | |
| Between horizontal and diagonal members | 55 | 51 | 48 | 45 | 42 | 40 | 38 | | | | | | | | | 10/n = tan a |
| Between diagonal and vertical members | 35 | 39 | 42 | 45 | 48 | 50 | 52 | | | | | | | | | 90 - a |
| Between vertical and horizontal members | 90 | 90 | 90 | 90 | 90 | 90 | 90 | | | | | | | | | 90 |

12 PANELS AT TOP & BOTTOM



$$N = \sqrt{n^2 + 144}$$

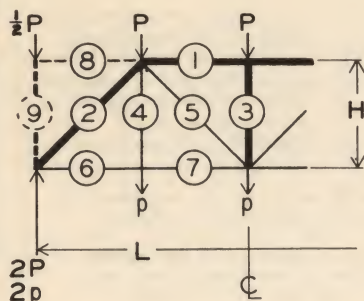
1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | | | | | | | | GENERAL FORMULAS | |
|---|-------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------------------|-----------|
| | 7 | 8 | 9 | 10 | 11 | 12 | 13 | | | | | | | | | |
| STRESS COEFFICIENTS | | | | | | | | | | | | | | | | |
| | P | p | P | p | P | p | P | p | P | p | P | p | P | p | P | p |
| 1 | - 3.21 | - 3.21 | - 3.67 | - 3.67 | - 4.13 | - 4.13 | - 4.58 | - 4.58 | - 5.04 | - 5.04 | - 5.50 | - 5.50 | - 5.96 | - 5.96 | - 11/24 n | - 11/24 n |
| 2 | - 5.83 | - 5.83 | - 6.67 | - 6.67 | - 7.50 | - 7.50 | - 8.33 | - 8.33 | - 9.17 | - 9.17 | -10.00 | -10.00 | -10.83 | -10.83 | - 20/24 n | - 20/24 n |
| 3 | - 7.88 | - 7.88 | - 9.00 | - 9.00 | -10.13 | -10.13 | -11.25 | -11.25 | -12.38 | -12.38 | -13.50 | -13.50 | -14.63 | -14.63 | - 27/24 n | - 27/24 n |
| 4 | - 9.33 | - 9.33 | -10.67 | -10.67 | -12.00 | -12.00 | -13.33 | -13.33 | -14.67 | -14.67 | -16.00 | -16.00 | -17.33 | -17.33 | - 32/24 n | - 32/24 n |
| 5 | -10.21 | -10.21 | -11.67 | -11.67 | -13.13 | -13.13 | -14.58 | -14.58 | -16.04 | -16.04 | -17.50 | -17.50 | -18.96 | -18.96 | - 35/24 n | - 35/24 n |
| 6 | -10.50 | -10.50 | -12.00 | -12.00 | -13.50 | -13.50 | -15.00 | -15.00 | -16.50 | -16.50 | -18.00 | -18.00 | -19.50 | -19.50 | - 36/24 n | - 36/24 n |
| 7 | - 5.50 | - 4.50 | - 5.50 | - 4.50 | - 5.50 | - 4.50 | - 5.50 | - 4.50 | - 5.50 | - 4.50 | - 5.50 | - 4.50 | - 5.50 | - 4.50 | - 11/2 | - 9/2 |
| 8 | - 4.50 | - 3.50 | - 4.50 | - 3.50 | - 4.50 | - 3.50 | - 4.50 | - 3.50 | - 4.50 | - 3.50 | - 4.50 | - 3.50 | - 4.50 | - 3.50 | - 9/2 | - 7/2 |
| 9 | - 3.50 | - 2.50 | - 3.50 | - 2.50 | - 3.50 | - 2.50 | - 3.50 | - 2.50 | - 3.50 | - 2.50 | - 3.50 | - 2.50 | - 3.50 | - 2.50 | - 7/2 | - 5/2 |
| 10 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 5/2 | - 3/2 |
| 11 | - 1.50 | - 0.50 | - 1.50 | - 0.50 | - 1.50 | - 0.50 | - 1.50 | - 0.50 | - 1.50 | - 0.50 | - 1.50 | - 0.50 | - 1.50 | - 0.50 | - 3/2 | - 1/2 |
| 12 | - 1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1 | 0 |
| 13 | 6.37 | 6.37 | 6.61 | 6.61 | 6.88 | 6.88 | 7.16 | 7.16 | 7.46 | 7.46 | 7.78 | 7.78 | 8.11 | 8.11 | 11/24 N | 11/24 N |
| 14 | 5.21 | 5.21 | 5.41 | 5.41 | 5.63 | 5.63 | 5.86 | 5.86 | 6.10 | 6.10 | 6.36 | 6.36 | 6.63 | 6.63 | 9/24 N | 9/24 N |
| 15 | 4.06 | 4.06 | 4.21 | 4.21 | 4.38 | 4.38 | 4.56 | 4.56 | 4.75 | 4.75 | 4.95 | 4.95 | 5.16 | 5.16 | 7/24 N | 7/24 N |
| 16 | 2.89 | 2.89 | 3.00 | 3.00 | 3.13 | 3.13 | 3.25 | 3.25 | 3.39 | 3.39 | 3.54 | 3.54 | 3.69 | 3.69 | 5/24 N | 5/24 N |
| 17 | 1.74 | 1.74 | 1.80 | 1.80 | 1.88 | 1.88 | 1.95 | 1.95 | 2.03 | 2.03 | 2.12 | 2.12 | 2.21 | 2.21 | 3/24 N | 3/24 N |
| 18 | 0.58 | 0.58 | 0.60 | 0.60 | 0.63 | 0.63 | 0.65 | 0.65 | 0.68 | 0.68 | 0.71 | 0.71 | 0.74 | 0.74 | 1/24 N | 1/24 N |
| 19 | 3.21 | 3.21 | 3.67 | 3.67 | 4.13 | 4.13 | 4.58 | 4.58 | 5.04 | 5.04 | 5.50 | 5.50 | 5.96 | 5.96 | 11/24 n | 11/24 n |
| 20 | 5.83 | 5.83 | 6.67 | 6.67 | 7.50 | 7.50 | 8.33 | 8.33 | 9.17 | 9.17 | 10.00 | 10.00 | 10.83 | 10.83 | 20/24 n | 20/24 n |
| 21 | 7.88 | 7.88 | 9.00 | 9.00 | 10.13 | 10.13 | 11.25 | 11.25 | 12.38 | 12.38 | 13.50 | 13.50 | 14.63 | 14.63 | 27/24 n | 27/24 n |
| 22 | 9.33 | 9.33 | 10.67 | 10.67 | 12.00 | 12.00 | 13.33 | 13.33 | 14.67 | 14.67 | 16.00 | 16.00 | 17.33 | 17.33 | 32/24 n | 32/24 n |
| 23 | 10.21 | 10.21 | 11.67 | 11.67 | 13.13 | 13.13 | 14.58 | 14.58 | 16.04 | 16.04 | 17.50 | 17.50 | 18.96 | 18.96 | 35/24 n | 35/24 n |
| 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 25 | - 6.00 | 0 | - 6.00 | 0 | - 6.00 | 0 | - 6.00 | 0 | - 6.00 | 0 | - 6.00 | 0 | - 6.00 | 0 | - 6 | 0 |
| LENGTH COEFFICIENTS | | | | | | | | | | | | | | | | |
| | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H |
| Horizontal | 0.583333 | 0.666667 | 0.750000 | 0.833333 | 0.916667 | 1.000000 | 1.083333 | 1.166667 | 1.250000 | 1.333333 | 1.416667 | 1.500000 | 1.583333 | 1.666667 | 1.750000 | 1.833333 |
| Diagonal | 1.157704 | 1.201850 | 1.250000 | 1.301708 | 1.356568 | 1.414214 | 1.474317 | 1.536864 | 1.601812 | 1.669160 | 1.738908 | 1.811056 | 1.885604 | 1.962552 | 2.041900 | 2.123648 |
| Vertical | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | | | | | | | | | |
| Between horizontal and diagonal members | 60 | 56 | 53 | 50 | 47 | 45 | 43 | 41 | 39 | 37 | 35 | 33 | 31 | 29 | 27 | 25 |
| Between diagonal and vertical members | 30 | 34 | 37 | 40 | 43 | 45 | 47 | 49 | 51 | 53 | 55 | 57 | 59 | 61 | 63 | 65 |
| Between vertical and horizontal members | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |

4 PANELS AT TOP & BOTTOM



$$n = \frac{1}{H}$$

$$N = \sqrt{n^2 + 16}$$

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

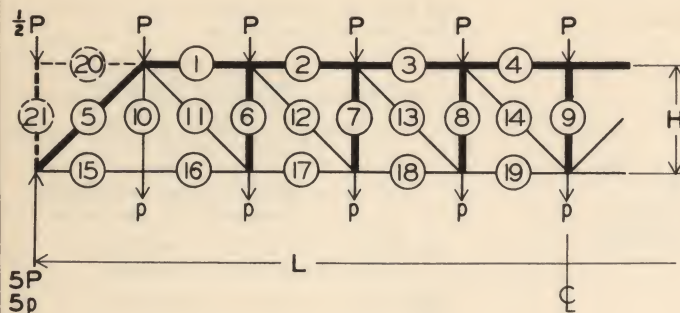
Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

[illegible]

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - MODIFIED FLAT PRATT

10 PANELS AT TOP & BOTTOM



$$n = \frac{L}{H}$$

$$N = \sqrt{n^2 + 100}$$

To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

ALL MEMBERS WHICH ARE IN COMPRESSION MUST BE DESIGNED AS COLUMNS

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | | | | | | | | GENERAL FORMULAS | |
|---------------------|-------------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------------------|-----------|
| | 7 | 8 | 9 | 10 | 11 | 12 | 13 | | | | | | | | | |
| STRESS COEFFICIENTS | | | | | | | | | | | | | | | | |
| | P | p | P | p | P | p | P | p | P | p | P | p | P | p | P | p |
| 1 | -5.60 | -5.60 | -6.40 | -6.40 | -7.20 | -7.20 | -8.00 | -8.00 | -8.80 | -8.80 | -9.60 | -9.60 | -10.40 | -10.40 | - 4/5 n | - 4/5 n |
| 2 | -7.35 | -7.35 | -8.40 | -8.40 | -9.45 | -9.45 | -10.50 | -10.50 | -11.55 | -11.55 | -12.60 | -12.60 | -13.65 | -13.65 | - 21/20 n | - 21/20 n |
| 3 | -8.40 | -8.40 | -9.60 | -9.60 | -10.80 | -10.80 | -12.00 | -12.00 | -13.20 | -13.20 | -14.40 | -14.40 | -15.60 | -15.60 | - 6/5 n | - 6/5 n |
| 4 | -8.75 | -8.75 | -10.00 | -10.00 | -11.25 | -11.25 | -12.50 | -12.50 | -13.75 | -13.75 | -15.00 | -15.00 | -16.25 | -16.25 | - 5/4 n | - 5/4 n |
| 5 | -5.49 | -5.49 | -5.76 | -5.76 | -6.05 | -6.05 | -6.36 | -6.36 | -6.69 | -6.69 | -7.03 | -7.03 | -7.38 | -7.38 | - 9/20 N | - 9/20 N |
| 6 | -3.50 | -2.50 | -3.50 | -2.50 | -3.50 | -2.50 | -3.50 | -2.50 | -3.50 | -2.50 | -3.50 | -2.50 | -3.50 | -2.50 | - 7/2 | - 5/2 |
| 7 | -2.50 | -1.50 | -2.50 | -1.50 | -2.50 | -1.50 | -2.50 | -1.50 | -2.50 | -1.50 | -2.50 | -1.50 | -2.50 | -1.50 | - 5/2 | - 3/2 |
| 8 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | -1.50 | -0.50 | - 3/2 | - 1/2 |
| 9 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | -1.00 | 0 | - 1 | 0 |
| 10 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1 |
| 11 | 4.27 | 4.27 | 4.48 | 4.48 | 4.71 | 4.71 | 4.95 | 4.95 | 5.20 | 5.20 | 5.47 | 5.47 | 5.74 | 5.74 | 7/20 N | 7/20 N |
| 12 | 3.05 | 3.05 | 3.20 | 3.20 | 3.36 | 3.36 | 3.54 | 3.54 | 3.72 | 3.72 | 3.91 | 3.91 | 4.10 | 4.10 | 1/4 N | 1/4 N |
| 13 | 1.83 | 1.83 | 1.92 | 1.92 | 2.02 | 2.02 | 2.12 | 2.12 | 2.23 | 2.23 | 2.34 | 2.34 | 2.46 | 2.46 | 3/20 N | 3/20 N |
| 14 | 0.61 | 0.61 | 0.64 | 0.64 | 0.67 | 0.67 | 0.71 | 0.71 | 0.74 | 0.74 | 0.78 | 0.78 | 0.82 | 0.82 | 1/20 N | 1/20 N |
| 15 | 3.15 | 3.15 | 3.60 | 3.60 | 4.05 | 4.05 | 4.50 | 4.50 | 4.95 | 4.95 | 5.40 | 5.40 | 5.85 | 5.85 | 9/20 n | 9/20 n |
| 16 | 3.15 | 3.15 | 3.60 | 3.60 | 4.05 | 4.05 | 4.50 | 4.50 | 4.95 | 4.95 | 5.40 | 5.40 | 5.85 | 5.85 | 9/20 n | 9/20 n |
| 17 | 5.60 | 5.60 | 6.40 | 6.40 | 7.20 | 7.20 | 8.00 | 8.00 | 8.80 | 8.80 | 9.60 | 9.60 | 10.40 | 10.40 | 4/5 n | 4/5 n |
| 18 | 7.35 | 7.35 | 8.40 | 8.40 | 9.45 | 9.45 | 10.50 | 10.50 | 11.55 | 11.55 | 12.60 | 12.60 | 13.65 | 13.65 | 21/20 n | 21/20 n |
| 19 | 8.40 | 8.40 | 9.60 | 9.60 | 10.80 | 10.80 | 12.00 | 12.00 | 13.20 | 13.20 | 14.40 | 14.40 | 15.60 | 15.60 | 6/5 n | 6/5 n |
| 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21 | -0.50 | 0 | -0.50 | 0 | -0.50 | 0 | -0.50 | 0 | -0.50 | 0 | -0.50 | 0 | -0.50 | 0 | - 1/2 | 0 |

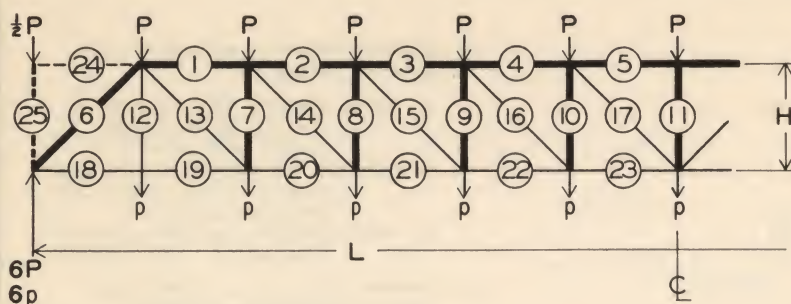
LENGTH COEFFICIENTS

| | H | H | H | H | H | H | H | H |
|------------|----------|----------|----------|----------|----------|----------|----------|----------|
| Horizontal | 0.700000 | 0.800000 | 0.900000 | 1.000000 | 1.100000 | 1.200000 | 1.300000 | 1/10 n |
| Diagonal | 1.220656 | 1.280625 | 1.345362 | 1.414214 | 1.486607 | 1.562050 | 1.640122 | 1/10 N |
| Vertical | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 |

ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS

| | | | | | | | | |
|---|----|----|----|----|----|----|----|-----------------|
| Between horizontal and diagonal members | 55 | 51 | 48 | 45 | 42 | 40 | 38 | 10/n = $\tan a$ |
| Between diagonal and vertical members | 35 | 39 | 42 | 45 | 48 | 50 | 52 | 90 - a |
| Between vertical and horizontal members | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |

12 PANELS AT TOP & BOTTOM



$$n = \frac{1}{H}$$

$$N = \sqrt{n^2 + 144}$$

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

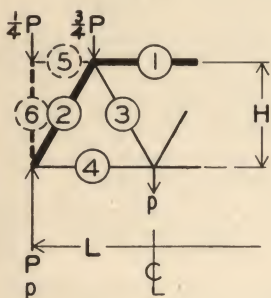
Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | | | | | | | | GENERAL FORMULAS | |
|---|-------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------------------|--------------|
| | 7 | 8 | 9 | 10 | 11 | 12 | 13 | | | | | | | | | |
| STRESS COEFFICIENTS | | | | | | | | | | | | | | | | |
| | P | p | P | p | P | p | P | p | P | p | P | p | P | p | P | p |
| 1 | - 5.83 | - 5.83 | - 6.67 | - 6.67 | - 7.50 | - 7.50 | - 8.33 | - 8.33 | - 9.17 | - 9.17 | -10.00 | -10.00 | -10.83 | -10.83 | - 20/24 n | - 20/24 n |
| 2 | - 7.88 | - 7.88 | - 9.00 | - 9.00 | -10.13 | -10.13 | -11.25 | -11.25 | -12.38 | -12.38 | -13.50 | -13.50 | -14.63 | -14.63 | - 27/24 n | - 27/24 n |
| 3 | - 9.33 | -9.33 | -10.67 | -10.67 | -12.00 | -12.00 | -13.33 | -13.33 | -14.67 | -14.67 | -16.00 | -16.00 | -17.33 | -17.33 | - 32/24 n | - 32/24 n |
| 4 | -10.21 | -10.21 | -11.67 | -11.67 | -13.13 | -13.13 | -14.58 | -14.58 | -16.04 | -16.04 | -17.50 | -17.50 | -18.96 | -18.96 | - 35/24 n | - 35/24 n |
| 5 | -10.50 | -10.50 | -12.00 | -12.00 | -13.50 | -13.50 | -15.00 | -15.00 | -16.50 | -16.50 | -18.00 | -18.00 | -19.50 | -19.50 | - 36/24 n | - 36/24 n |
| 6 | - 6.37 | - 6.37 | - 6.61 | - 6.61 | - 6.88 | - 6.88 | - 7.16 | - 7.16 | - 7.46 | - 7.46 | - 7.78 | - 7.78 | - 8.11 | - 8.11 | - 11/24 N | - 11/24 N |
| 7 | - 4.50 | - 3.50 | - 4.50 | - 3.50 | - 4.50 | - 3.50 | - 4.50 | - 3.50 | - 4.50 | - 3.50 | - 4.50 | - 3.50 | - 4.50 | - 3.50 | - 9/2 | - 7/2 |
| 8 | - 3.50 | - 2.50 | - 3.50 | - 2.50 | - 3.50 | - 2.50 | - 3.50 | - 2.50 | - 3.50 | - 2.50 | - 3.50 | - 2.50 | - 3.50 | - 2.50 | - 7/2 | - 5/2 |
| 9 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 2.50 | - 1.50 | - 5/2 | - 3/2 |
| 10 | - 1.50 | - 0.50 | - 1.50 | - 0.50 | - 1.50 | - 0.50 | - 1.50 | - 0.50 | - 1.50 | - 0.50 | - 1.50 | - 0.50 | - 1.50 | - 0.50 | - 3/2 | - 1/2 |
| 11 | - 1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1.00 | 0 | - 1 | 0 |
| 12 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1.00 | 0 | 1 |
| 13 | 5.21 | 5.21 | 5.41 | 5.41 | 5.63 | 5.63 | 5.86 | 5.86 | 6.10 | 6.10 | 6.36 | 6.36 | 6.65 | 6.65 | 9/24 N | 9/24 N |
| 14 | 4.05 | 4.05 | 4.21 | 4.21 | 4.38 | 4.38 | 4.56 | 4.56 | 4.75 | 4.75 | 4.95 | 4.95 | 5.16 | 5.16 | 7/24 N | 7/24 N |
| 15 | 2.89 | 2.89 | 3.00 | 3.00 | 3.13 | 3.13 | 3.25 | 3.25 | 3.39 | 3.39 | 3.54 | 3.54 | 3.69 | 3.69 | 5/24 N | 5/24 N |
| 16 | 1.74 | 1.74 | 1.80 | 1.80 | 1.88 | 1.88 | 1.95 | 1.95 | 2.03 | 2.03 | 2.12 | 2.12 | 2.21 | 2.21 | 3/24 N | 3/24 N |
| 17 | 0.58 | 0.58 | 0.60 | 0.60 | 0.63 | 0.63 | 0.65 | 0.65 | 0.68 | 0.68 | 0.71 | 0.71 | 0.74 | 0.74 | 1/24 N | 1/24 N |
| 18 | 3.21 | 3.21 | 3.67 | 3.67 | 4.13 | 4.13 | 4.58 | 4.58 | 5.04 | 5.04 | 5.50 | 5.50 | 5.96 | 5.96 | 11/24 n | 11/24 n |
| 19 | 3.21 | 3.21 | 3.67 | 3.67 | 4.13 | 4.13 | 4.58 | 4.58 | 5.04 | 5.04 | 5.50 | 5.50 | 5.96 | 5.96 | 11/24 n | 11/24 n |
| 20 | 5.83 | 5.83 | 6.67 | 6.67 | 7.50 | 7.50 | 8.33 | 8.33 | 9.17 | 9.17 | 10.00 | 10.00 | 10.83 | 10.83 | 20/24 n | 20/24 n |
| 21 | 7.88 | 7.88 | 9.00 | 9.00 | 10.13 | 10.13 | 11.25 | 11.25 | 12.38 | 12.38 | 13.50 | 13.50 | 14.63 | 14.63 | 27/24 n | 27/24 n |
| 22 | 9.33 | 9.33 | 10.67 | 10.67 | 12.00 | 12.00 | 13.33 | 13.33 | 14.67 | 14.67 | 16.00 | 16.00 | 17.33 | 17.33 | 32/24 n | 32/24 n |
| 23 | 10.21 | 10.21 | 11.67 | 11.67 | 13.13 | 13.13 | 14.58 | 14.58 | 16.04 | 16.04 | 17.50 | 17.50 | 18.96 | 18.96 | 35/24 n | 35/24 n |
| 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 25 | - 0.50 | 0 | - 0.50 | 0 | - 0.50 | 0 | - 0.50 | 0 | - 0.50 | 0 | - 0.50 | 0 | - 0.50 | 0 | - 1/2 | 0 |
| LENGTH COEFFICIENTS | | | | | | | | | | | | | | | | |
| | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H |
| Horizontal | 0.583333 | 0.666667 | 0.750000 | 0.833333 | 0.916667 | 1.000000 | 1.083333 | 1.166667 | 1.250000 | 1.333333 | 1.416667 | 1.500000 | 1.583333 | 1.666667 | 1.750000 | 1/12 n |
| Diagonal | 1.157704 | 1.201850 | 1.250000 | 1.301708 | 1.356568 | 1.414214 | 1.474317 | 1.536875 | 1.601896 | 1.670381 | 1.742331 | 1.817746 | 1.896626 | 1.978971 | 2.064891 | 1/12 N |
| Vertical | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | | | | | | | | | |
| Between horizontal and diagonal members | 60 | 56 ° | 53 | 50 | 47 | 45 | 43 | 41 | 39 | 37 | 35 | 33 | 31 | 29 | 27 | 12/n = tan a |
| Between diagonal and vertical members | 30 | 34 | 37 | 40 | 43 | 45 | 47 | 49 | 51 | 53 | 55 | 57 | 59 | 61 | 63 | 90 - a |
| Between vertical and horizontal members | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - FLAT WARREN

2 PANELS AT BOTTOM



$$n = \frac{L}{H}$$

$$N = \sqrt{n^2 + 16}$$

To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

ALL MEMBERS WHICH ARE IN COMPRESSION MUST BE DESIGNED AS COLUMNS

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | | | | | | | | GENERAL FORMULAS | |
|---|-------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|------------------|---------|
| | 7 | 8 | 9 | 10 | 11 | 12 | 13 | | | | | | | | | |
| STRESS COEFFICIENTS | | | | | | | | | | | | | | | | |
| | P | p | P | p | P | p | P | p | P | p | P | p | P | p | P | p |
| 1 | -1.31 | -1.75 | -1.50 | -2.00 | -1.69 | -2.25 | -1.88 | -2.50 | -2.06 | -2.75 | -2.25 | -3.00 | -2.44 | -3.25 | - 3/16 n | - 1/4 n |
| 2 | -1.51 | -1.01 | -1.68 | -1.12 | -1.85 | -1.23 | -2.02 | -1.35 | -2.19 | -1.43 | -2.37 | -1.58 | -2.55 | -1.70 | - 3/16 N | - 1/8 N |
| 3 | 0 | 1.01 | 0 | 1.12 | 0 | 1.23 | 0 | 1.35 | 0 | 1.46 | 0 | 1.58 | 0 | 1.70 | 0 | 1/8 N |
| 4 | 1.31 | 0.88 | 1.50 | 1.00 | 1.69 | 1.13 | 1.88 | 1.25 | 2.06 | 1.38 | 2.25 | 1.50 | 2.44 | 1.63 | 3/16 n | 1/8 n |
| 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | - 1/4 | 0 |
| LENGTH COEFFICIENTS | | | | | | | | | | | | | | | | |
| | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H |
| 1, 4 | 3.500000 | 4.000000 | 4.500000 | 5.000000 | 5.500000 | 6.000000 | 6.500000 | 7.000000 | 7.500000 | 8.000000 | 8.500000 | 9.000000 | 9.500000 | 10.000000 | 1/2 n | |
| 2, 3 | 2.015564 | 2.236068 | 2.462214 | 2.692582 | 2.926175 | 3.162278 | 3.400368 | 3.640368 | 3.882278 | 4.126175 | 4.372278 | 4.620368 | 4.870368 | 5.122278 | 1/4 N | |
| 5 | 1.750000 | 2.000000 | 2.250000 | 2.500000 | 2.750000 | 3.000000 | 3.250000 | 3.500000 | 3.750000 | 4.000000 | 4.250000 | 4.500000 | 4.750000 | 5.000000 | 1/4 n | |
| 6 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 | |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | | | | | | | | | |
| Between horizontal and diagonal members | 50 | 27 | 24 | 22 | 20 | 18 | 17 | | | | | | | | 4/n = tan a | |
| Between diagonal members | 120 | 126 | 132 | 136 | 140 | 144 | 146 | | | | | | | | 180 - 2a | |
| Between vertical and diagonal members | 60 | 63 | 66 | 68 | 70 | 72 | 73 | | | | | | | | 90 - a | |
| Between vertical and horizontal members | 90 | 90 | 90 | 90 | 90 | 90 | 90 | | | | | | | | 90 | |

[illegible]

$$n = \frac{1}{H}$$

$$N = \sqrt{n^2 + 36}$$

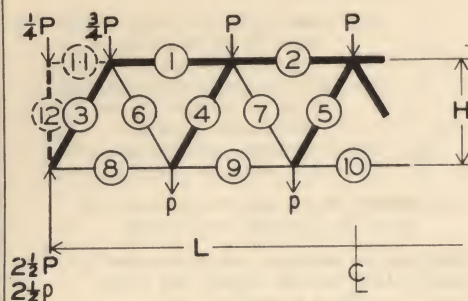
1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

[illegible]

5 PANELS AT BOTTOM



$$n = \frac{1}{H} \cdot$$

$$N = \sqrt{n^2 + 100}$$

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

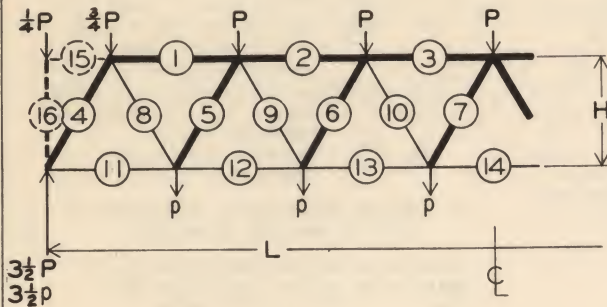
Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

[illegible]

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - FLAT WARREN

7 PANELS AT BOTTOM



$$n = \frac{L}{H}$$

$$N = \sqrt{n^2 + 196}$$

To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

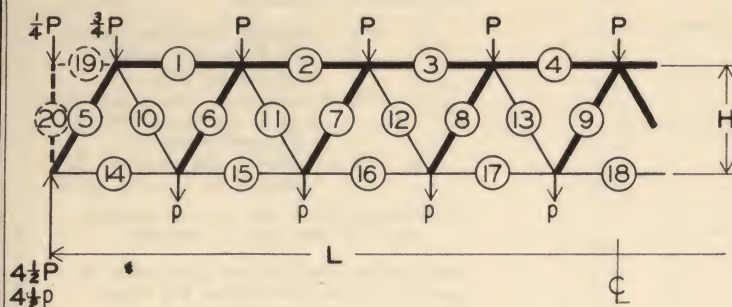
ALL MEMBERS WHICH ARE IN COMPRESSION MUST BE DESIGNED AS COLUMNS

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

| MEMBER | VALUES OF n | | | | | | | | | | | | | | GENERAL FORMULAS | |
|---|-------------|----------|----------|----------|----------|----------|----------|-------|-------|-------|--------|--------|--------|--------|------------------|--------------|
| | 7 | 8 | 9 | 10 | 11 | 12 | 13 | | | | | | | | | |
| STRESS COEFFICIENTS | | | | | | | | | | | | | | | | |
| | P | p | P | p | P | p | P | p | P | p | P | p | P | p | P | p |
| 1 | -2.88 | -3.00 | -3.29 | -3.43 | -3.70 | -3.86 | -4.11 | -4.29 | -4.52 | -4.71 | -4.93 | -5.14 | -5.34 | -5.57 | - 23/56 n | - 24/56 n |
| 2 | -4.88 | -5.00 | -5.57 | -5.71 | -6.27 | -6.43 | -6.96 | -7.14 | -7.66 | -7.86 | -8.36 | -8.57 | -9.05 | -9.29 | - 39/56 n | - 40/56 n |
| 3 | -5.88 | -6.00 | -6.71 | -6.86 | -7.55 | -7.71 | -8.39 | -8.57 | -9.23 | -9.43 | -10.07 | -10.29 | -10.91 | -11.14 | - 47/56 n | - 48/56 n |
| 4 | -3.63 | -3.55 | -3.74 | -3.46 | -3.86 | -3.57 | -3.99 | -3.69 | -4.13 | -3.82 | -4.28 | -3.95 | -4.44 | -4.09 | - 13/56 N | - 12/56 N |
| 5 | -2.80 | -2.24 | -2.88 | -2.50 | -2.97 | -2.38 | -3.07 | -2.46 | -3.18 | -2.54 | -3.29 | -2.63 | -3.41 | -2.73 | - 10/56 N | - 8/56 N |
| 6 | -1.68 | -1.12 | -1.73 | -1.15 | -1.78 | -1.19 | -1.84 | -1.23 | -1.91 | -1.27 | -1.98 | -1.32 | -2.05 | -1.36 | - 6/56 N | - 4/56 N |
| 7 | -0.56 | 0 | -0.58 | 0 | -0.59 | 0 | -0.61 | 0 | -0.64 | 0 | -0.66 | 0 | -0.68 | 0 | - 2/56 N | 0 |
| 8 | 2.80 | 3.35 | 2.88 | 3.46 | 2.97 | 3.57 | 3.07 | 3.69 | 3.18 | 3.82 | 3.29 | 3.95 | 3.41 | 4.09 | 10/56 N | 12/56 N |
| 9 | 1.68 | 2.24 | 1.73 | 2.50 | 1.78 | 2.38 | 1.84 | 2.46 | 1.91 | 2.54 | 1.98 | 2.63 | 2.05 | 2.73 | 6/56 N | 8/56 N |
| 10 | 0.56 | 1.12 | 0.58 | 1.15 | 0.59 | 1.19 | 0.61 | 1.23 | 0.64 | 1.27 | 0.66 | 1.32 | 0.68 | 1.36 | 2/56 N | 4/56 N |
| 11 | 1.63 | 1.50 | 1.86 | 1.71 | 2.09 | 1.93 | 2.32 | 2.34 | 2.55 | 2.36 | 2.79 | 2.57 | 3.02 | 2.79 | 13/56 n | 12/56 n |
| 12 | 4.13 | 4.00 | 4.71 | 4.57 | 5.30 | 5.14 | 5.89 | 5.71 | 6.48 | 6.29 | 7.07 | 6.86 | 7.66 | 7.43 | 33/56 n | 32/56 n |
| 13 | 5.63 | 5.50 | 6.43 | 6.29 | 7.23 | 7.07 | 8.04 | 7.86 | 8.84 | 8.64 | 9.64 | 9.43 | 10.45 | 10.21 | 45/56 n | 44/56 n |
| 14 | 6.13 | 6.00 | 7.00 | 6.86 | 7.88 | 7.71 | 8.75 | 8.57 | 9.63 | 9.43 | 10.50 | 10.29 | 11.38 | 11.14 | 49/56 n | 48/56 n |
| 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | - 1/4 | 0 |
| LENGTH COEFFICIENTS | | | | | | | | | | | | | | | | |
| | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H |
| 1, 2, 3, 11, 12, 13, 14 | 1.000000 | 1.142857 | 1.285714 | 1.428571 | 1.571429 | 1.714286 | 1.857143 | | | | | | | | | 1/7 n |
| 4, 5, 6, 7, 8, 9, 10 | 1.118034 | 1.151751 | 1.188808 | 1.228904 | 1.271750 | 1.317078 | 1.364641 | | | | | | | | | 1/14 N |
| 15 | 0.500000 | 0.571429 | 0.642857 | 0.714286 | 0.785714 | 0.857143 | 0.928571 | | | | | | | | | 1/14 n |
| 16 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | | | | | | | | | 1 |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | | | | | | | | | |
| Between horizontal and diagonal members | 63 | 60 | 57 | 54 | 52 | 49 | 47 | | | | | | | | | 14/n = tan a |
| Between diagonal members | 54 | 60 | 66 | 72 | 76 | 82 | 86 | | | | | | | | | 180 - 2a |
| Between diagonal and vertical members | 27 | 30 | 33 | 36 | 38 | 41 | 45 | | | | | | | | | 90 - a |
| Between vertical and horizontal members | 90 | 90 | 90 | 90 | 90 | 90 | 90 | | | | | | | | | 90 |

TRUSSES - STRESS COEFFICIENTS, LENGTH COEFFICIENTS, & ANGLES - FLAT WARREN
9 PANELS AT BOTTOM



To find the stress in any member when the truss is loaded at:

1. TOP - multiply the panel point load P by the stress coefficient under P
2. BOTTOM - multiply the panel point load p by the stress coefficient under p
3. TOP & BOTTOM - add stresses determined in 1 and 2 above

ALL MEMBERS WHICH ARE IN COMPRESSION
MUST BE DESIGNED AS COLUMNS

Compressive members are designated by heavy lines on the sketch and minus sign (-) before coefficients.

To find the length of any member, multiply the height of truss H by the length coefficient under H .

$$n = \frac{L}{H}$$

$$N = \sqrt{n^2 + 324}$$

| MEMBER | VALUES OF n | | | | | | | | | | | | | | GENERAL FORMULAS | |
|---|-------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------------------|--------------|
| | 7 | 8 | 9 | 10 | 11 | 12 | 13 | | | | | | | | | |
| STRESS COEFFICIENTS | | | | | | | | | | | | | | | | |
| | P | p | P | p | P | p | P | p | P | p | P | p | P | p | P | p |
| 1 | -3.01 | -3.11 | -3.44 | -3.56 | -3.88 | -4.00 | -4.31 | -4.44 | -4.74 | -4.89 | -5.17 | -5.33 | -5.60 | -5.78 | - 31/72 n | - 32/72 n |
| 2 | -5.35 | -5.44 | -6.11 | -6.22 | -6.88 | -7.00 | -7.64 | -7.78 | -8.40 | -8.56 | -9.17 | -9.33 | -9.93 | -10.11 | - 55/72 n | - 56/72 n |
| 3 | -6.90 | -7.00 | -7.89 | -8.00 | -8.88 | -9.00 | -9.86 | -10.00 | -10.85 | -11.00 | -11.83 | -12.00 | -12.82 | -13.00 | - 71/72 n | - 72/72 n |
| 4 | -7.68 | -7.78 | -8.78 | -8.89 | -9.88 | -10.00 | -10.97 | -11.11 | -12.07 | -12.22 | -13.17 | -13.33 | -14.26 | -14.44 | - 79/72 n | - 80/72 n |
| 5 | -4.56 | -4.29 | -4.65 | -4.38 | -4.75 | -4.47 | -4.86 | -4.58 | -4.98 | -4.69 | -5.11 | -4.81 | -5.24 | -4.93 | - 17/72 N | - 16/72 N |
| 6 | -3.76 | -3.22 | -3.83 | -3.28 | -3.91 | -3.35 | -4.00 | -3.43 | -4.10 | -3.52 | -4.21 | -3.61 | -4.32 | -3.70 | - 14/72 N | - 12/72 N |
| 7 | -2.68 | -2.15 | -2.74 | -2.19 | -2.80 | -2.24 | -2.86 | -2.29 | -2.93 | -2.34 | -3.00 | -2.40 | -3.08 | -2.47 | - 10/72 N | - 8/72 N |
| 8 | -1.61 | -1.07 | -1.64 | -1.09 | -1.68 | -1.12 | -1.72 | -1.14 | -1.76 | -1.17 | -1.80 | -1.20 | -1.85 | -1.23 | - 6/72 N | - 4/72 N |
| 9 | -0.54 | 0 | -0.55 | 0 | -0.56 | 0 | -0.57 | 0 | -0.59 | 0 | -0.60 | 0 | -0.62 | 0 | - 2/72 N | 0 |
| 10 | 3.76 | 4.29 | 3.83 | 4.38 | 3.91 | 4.47 | 4.00 | 4.58 | 4.10 | 4.69 | 4.21 | 4.81 | 4.32 | 4.93 | 14/72 N | 16/72 N |
| 11 | 2.68 | 3.22 | 2.74 | 3.28 | 2.80 | 3.35 | 2.86 | 3.43 | 2.93 | 3.52 | 3.00 | 3.61 | 3.08 | 3.70 | 10/72 N | 12/72 N |
| 12 | 1.61 | 2.15 | 1.64 | 2.19 | 1.68 | 2.24 | 1.72 | 2.29 | 1.76 | 2.34 | 1.80 | 2.40 | 1.85 | 2.47 | 6/72 N | 8/72 N |
| 13 | 0.54 | 1.07 | 0.55 | 1.09 | 0.56 | 1.12 | 0.57 | 1.14 | 0.59 | 1.17 | 0.60 | 1.20 | 0.62 | 1.23 | 2/72 N | 4/72 N |
| 14 | 1.65 | 1.56 | 1.89 | 1.78 | 2.13 | 2.00 | 2.36 | 2.22 | 2.60 | 2.44 | 2.83 | 2.67 | 3.07 | 2.89 | 17/72 n | 16/72 n |
| 15 | 4.38 | 4.28 | 5.00 | 4.89 | 5.63 | 5.50 | 6.25 | 6.11 | 6.88 | 6.72 | 7.50 | 7.33 | 8.13 | 7.94 | 45/72 n | 44/72 n |
| 16 | 6.32 | 6.22 | 7.22 | 7.11 | 8.13 | 8.00 | 9.03 | 8.89 | 9.93 | 9.78 | 10.83 | 10.67 | 11.74 | 11.56 | 65/72 n | 64/72 n |
| 17 | 7.49 | 7.39 | 8.56 | 8.44 | 9.63 | 9.50 | 10.69 | 10.56 | 11.76 | 11.61 | 12.83 | 12.67 | 13.90 | 13.72 | 77/72 n | 76/72 n |
| 18 | 7.88 | 7.78 | 9.00 | 8.89 | 10.13 | 10.00 | 11.25 | 11.11 | 12.38 | 12.22 | 13.50 | 13.33 | 14.63 | 14.44 | 81/72 n | 80/72 n |
| 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | -0.25 | 0 | - 1/4 | 0 |
| LENGTH COEFFICIENTS | | | | | | | | | | | | | | | | |
| | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H | H |
| 1, 2, 3, 4, 14, 15, 16, 17, 18 | 0.777778 | 0.888889 | 1.000000 | 1.111111 | 1.222222 | 1.333333 | 1.444444 | 1.555555 | 1.666667 | 1.777778 | 1.888889 | 2.000000 | 2.111111 | 2.222222 | 2.333333 | 1/9 n |
| 5, 6, 7, 8, 9, 10, 11, 12, 13 | 1.072956 | 1.094318 | 1.118034 | 1.143959 | 1.171946 | 1.201850 | 1.233534 | 1.266667 | 1.300000 | 1.333333 | 1.366667 | 1.400000 | 1.433333 | 1.466667 | 1.500000 | 1/18 N |
| 19 | 0.388889 | 0.444444 | 0.500000 | 0.555556 | 0.611111 | 0.666667 | 0.722222 | 0.777778 | 0.833333 | 0.888889 | 0.944444 | 1.000000 | 1.055556 | 1.111111 | 1.166667 | 1/18 n |
| 20 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1.000000 | 1 |
| ANGLES (IN DEGREES) BETWEEN MEMBERS FOR USE IN DETERMINING BOLT AND CONNECTOR LOADS | | | | | | | | | | | | | | | | |
| Between horizontal and diagonal members | 69 | 66 | 63 | 61 | 59 | 56 | 54 | 52 | 50 | 48 | 46 | 44 | 42 | 40 | 38 | 18/n = tan a |
| Between diagonal members | 42 | 48 | 54 | 58 | 62 | 68 | 72 | 78 | 84 | 90 | 96 | 102 | 108 | 114 | 120 | 180 - 2a |
| Between diagonal and vertical members | 21 | 24 | 27 | 29 | 31 | 34 | 36 | 39 | 42 | 46 | 50 | 54 | 58 | 62 | 66 | 90 - a |
| Between vertical and horizontal members | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |

WOOD STRUCTURAL DESIGN DATA

DECIMAL EQUIVALENTS

DECIMALS OF A FOOT

DECIMALS OF AN INCH

| FRACTION | DECIMAL | FRACTION | DECIMAL | FRACTION | DECIMAL | FRACTION | DECIMAL |
|------------------|---------|------------------|---------|-------------------|---------|-----------------|----------|
| $\frac{1}{16}$ | 0.0052 | $4\frac{1}{16}$ | 0.3385 | $8\frac{1}{16}$ | 0.6719 | $\frac{1}{64}$ | 0.015625 |
| $\frac{1}{8}$ | 0.0104 | $4\frac{1}{8}$ | 0.3438 | $8\frac{1}{8}$ | 0.6771 | $\frac{1}{32}$ | 0.03125 |
| $\frac{3}{16}$ | 0.0156 | $4\frac{3}{16}$ | 0.3490 | $8\frac{3}{16}$ | 0.6823 | $\frac{3}{64}$ | 0.046875 |
| $\frac{1}{4}$ | 0.0208 | $4\frac{1}{4}$ | 0.3542 | $8\frac{1}{4}$ | 0.6875 | $\frac{1}{16}$ | 0.0625 |
| $\frac{5}{16}$ | 0.0260 | $4\frac{5}{16}$ | 0.3594 | $8\frac{5}{16}$ | 0.6927 | $\frac{5}{64}$ | 0.078125 |
| $\frac{3}{8}$ | 0.0313 | $4\frac{3}{8}$ | 0.3646 | $8\frac{3}{8}$ | 0.6979 | $\frac{3}{32}$ | 0.09375 |
| $\frac{7}{16}$ | 0.0365 | $4\frac{7}{16}$ | 0.3698 | $8\frac{7}{16}$ | 0.7031 | $\frac{7}{64}$ | 0.109375 |
| $\frac{1}{2}$ | 0.0417 | $4\frac{1}{2}$ | 0.3750 | $8\frac{1}{2}$ | 0.7083 | $\frac{1}{8}$ | 0.125 |
| $\frac{9}{16}$ | 0.0469 | $4\frac{9}{16}$ | 0.3802 | $8\frac{9}{16}$ | 0.7135 | $\frac{9}{64}$ | 0.140625 |
| $\frac{5}{8}$ | 0.0521 | $4\frac{5}{8}$ | 0.3854 | $8\frac{5}{8}$ | 0.7188 | $\frac{5}{32}$ | 0.15625 |
| $\frac{11}{16}$ | 0.0573 | $4\frac{11}{16}$ | 0.3906 | $8\frac{11}{16}$ | 0.7240 | $\frac{11}{64}$ | 0.171875 |
| $\frac{3}{4}$ | 0.0625 | $4\frac{3}{4}$ | 0.3958 | $8\frac{3}{4}$ | 0.7292 | $\frac{3}{16}$ | 0.1875 |
| $\frac{13}{16}$ | 0.0677 | $4\frac{13}{16}$ | 0.4010 | $8\frac{13}{16}$ | 0.7344 | $\frac{13}{64}$ | 0.203125 |
| $\frac{7}{8}$ | 0.0729 | $4\frac{7}{8}$ | 0.4063 | $8\frac{7}{8}$ | 0.7396 | $\frac{7}{32}$ | 0.21875 |
| $\frac{15}{16}$ | 0.0781 | $4\frac{15}{16}$ | 0.4115 | $8\frac{15}{16}$ | 0.7448 | $\frac{15}{64}$ | 0.234375 |
| 1- | 0.0833 | 5- | 0.4167 | 9- | 0.7500 | $\frac{1}{4}$ | 0.250 |
| $1\frac{1}{16}$ | 0.0885 | $5\frac{1}{16}$ | 0.4219 | $9\frac{1}{16}$ | 0.7552 | $\frac{17}{64}$ | 0.265625 |
| $1\frac{1}{8}$ | 0.0938 | $5\frac{1}{8}$ | 0.4271 | $9\frac{1}{8}$ | 0.7604 | $\frac{9}{32}$ | 0.28125 |
| $1\frac{3}{16}$ | 0.0990 | $5\frac{3}{16}$ | 0.4323 | $9\frac{3}{16}$ | 0.7656 | $\frac{19}{64}$ | 0.296875 |
| $1\frac{1}{4}$ | 0.1042 | $5\frac{1}{4}$ | 0.4375 | $9\frac{1}{4}$ | 0.7708 | $\frac{5}{16}$ | 0.3125 |
| $1\frac{5}{16}$ | 0.1094 | $5\frac{5}{16}$ | 0.4427 | $9\frac{5}{16}$ | 0.7760 | $\frac{21}{64}$ | 0.328125 |
| $1\frac{3}{8}$ | 0.1146 | $5\frac{3}{8}$ | 0.4479 | $9\frac{3}{8}$ | 0.7813 | $\frac{11}{32}$ | 0.34375 |
| $1\frac{7}{16}$ | 0.1198 | $5\frac{7}{16}$ | 0.4531 | $9\frac{7}{16}$ | 0.7865 | $\frac{23}{64}$ | 0.359375 |
| $1\frac{1}{2}$ | 0.1250 | $5\frac{1}{2}$ | 0.4583 | $9\frac{1}{2}$ | 0.7917 | $\frac{3}{8}$ | 0.375 |
| $1\frac{9}{16}$ | 0.1302 | $5\frac{9}{16}$ | 0.4635 | $9\frac{9}{16}$ | 0.7969 | $\frac{25}{64}$ | 0.390625 |
| $1\frac{5}{8}$ | 0.1354 | $5\frac{5}{8}$ | 0.4688 | $9\frac{5}{8}$ | 0.8021 | $\frac{13}{32}$ | 0.40625 |
| $1\frac{11}{16}$ | 0.1406 | $5\frac{11}{16}$ | 0.4740 | $9\frac{11}{16}$ | 0.8073 | $\frac{27}{64}$ | 0.421875 |
| $1\frac{3}{4}$ | 0.1458 | $5\frac{3}{4}$ | 0.4792 | $9\frac{3}{4}$ | 0.8125 | $\frac{7}{16}$ | 0.4375 |
| $1\frac{13}{16}$ | 0.1510 | $5\frac{13}{16}$ | 0.4844 | $9\frac{13}{16}$ | 0.8177 | $\frac{29}{64}$ | 0.453125 |
| $1\frac{7}{8}$ | 0.1563 | $5\frac{7}{8}$ | 0.4896 | $9\frac{7}{8}$ | 0.8229 | $\frac{15}{32}$ | 0.46875 |
| $1\frac{15}{16}$ | 0.1615 | $5\frac{15}{16}$ | 0.4948 | $9\frac{15}{16}$ | 0.8281 | $\frac{31}{64}$ | 0.484375 |
| 2- | 0.1667 | 6- | 0.5000 | 10- | 0.8333 | $\frac{1}{2}$ | 0.500 |
| $2\frac{1}{16}$ | 0.1719 | $6\frac{1}{16}$ | 0.5052 | $10\frac{1}{16}$ | 0.8385 | $\frac{33}{64}$ | 0.515625 |
| $2\frac{1}{8}$ | 0.1771 | $6\frac{1}{8}$ | 0.5104 | $10\frac{1}{8}$ | 0.8438 | $\frac{17}{32}$ | 0.53125 |
| $2\frac{3}{16}$ | 0.1823 | $6\frac{3}{16}$ | 0.5156 | $10\frac{3}{16}$ | 0.8490 | $\frac{35}{64}$ | 0.546875 |
| $2\frac{1}{4}$ | 0.1875 | $6\frac{1}{4}$ | 0.5208 | $10\frac{1}{4}$ | 0.8542 | $\frac{9}{16}$ | 0.5625 |
| $2\frac{5}{16}$ | 0.1927 | $6\frac{5}{16}$ | 0.5260 | $10\frac{5}{16}$ | 0.8594 | $\frac{37}{64}$ | 0.578125 |
| $2\frac{3}{8}$ | 0.1979 | $6\frac{3}{8}$ | 0.5313 | $10\frac{3}{8}$ | 0.8646 | $\frac{19}{32}$ | 0.59375 |
| $2\frac{7}{16}$ | 0.2031 | $6\frac{7}{16}$ | 0.5365 | $10\frac{7}{16}$ | 0.8698 | $\frac{39}{64}$ | 0.609375 |
| $2\frac{1}{2}$ | 0.2083 | $6\frac{1}{2}$ | 0.5417 | $10\frac{1}{2}$ | 0.8750 | $\frac{5}{8}$ | 0.625 |
| $2\frac{9}{16}$ | 0.2135 | $6\frac{9}{16}$ | 0.5469 | $10\frac{9}{16}$ | 0.8802 | $\frac{41}{64}$ | 0.640625 |
| $2\frac{5}{8}$ | 0.2188 | $6\frac{5}{8}$ | 0.5521 | $10\frac{5}{8}$ | 0.8854 | $\frac{21}{32}$ | 0.65625 |
| $2\frac{11}{16}$ | 0.2240 | $6\frac{11}{16}$ | 0.5573 | $10\frac{11}{16}$ | 0.8906 | $\frac{43}{64}$ | 0.671875 |
| $2\frac{3}{4}$ | 0.2292 | $6\frac{3}{4}$ | 0.5625 | $10\frac{3}{4}$ | 0.8958 | $\frac{11}{16}$ | 0.6875 |
| $2\frac{13}{16}$ | 0.2344 | $6\frac{13}{16}$ | 0.5677 | $10\frac{13}{16}$ | 0.9010 | $\frac{45}{64}$ | 0.703125 |
| $2\frac{7}{8}$ | 0.2396 | $6\frac{7}{8}$ | 0.5729 | $10\frac{7}{8}$ | 0.9063 | $\frac{23}{32}$ | 0.71875 |
| $2\frac{15}{16}$ | 0.2448 | $6\frac{15}{16}$ | 0.5781 | $10\frac{15}{16}$ | 0.9115 | $\frac{47}{64}$ | 0.734375 |
| 3- | 0.2500 | 7- | 0.5833 | 11- | 0.9167 | $\frac{3}{4}$ | 0.750 |
| $3\frac{1}{16}$ | 0.2552 | $7\frac{1}{16}$ | 0.5885 | $11\frac{1}{16}$ | 0.9219 | $\frac{49}{64}$ | 0.765625 |
| $3\frac{1}{8}$ | 0.2604 | $7\frac{1}{8}$ | 0.5938 | $11\frac{1}{8}$ | 0.9271 | $\frac{25}{32}$ | 0.78125 |
| $3\frac{3}{16}$ | 0.2656 | $7\frac{3}{16}$ | 0.5990 | $11\frac{3}{16}$ | 0.9323 | $\frac{51}{64}$ | 0.796875 |
| $3\frac{1}{4}$ | 0.2708 | $7\frac{1}{4}$ | 0.6042 | $11\frac{1}{4}$ | 0.9375 | $\frac{13}{16}$ | 0.8125 |
| $3\frac{5}{16}$ | 0.2760 | $7\frac{5}{16}$ | 0.6094 | $11\frac{5}{16}$ | 0.9427 | $\frac{53}{64}$ | 0.828125 |
| $3\frac{3}{8}$ | 0.2813 | $7\frac{3}{8}$ | 0.6146 | $11\frac{3}{8}$ | 0.9479 | $\frac{27}{32}$ | 0.84375 |
| $3\frac{7}{16}$ | 0.2865 | $7\frac{7}{16}$ | 0.6198 | $11\frac{7}{16}$ | 0.9531 | $\frac{55}{64}$ | 0.859375 |
| $3\frac{1}{2}$ | 0.2917 | $7\frac{1}{2}$ | 0.6250 | $11\frac{1}{2}$ | 0.9583 | $\frac{7}{8}$ | 0.875 |
| $3\frac{9}{16}$ | 0.2969 | $7\frac{9}{16}$ | 0.6302 | $11\frac{9}{16}$ | 0.9635 | $\frac{57}{64}$ | 0.890625 |
| $3\frac{5}{8}$ | 0.3021 | $7\frac{5}{8}$ | 0.6354 | $11\frac{5}{8}$ | 0.9688 | $\frac{29}{32}$ | 0.90625 |
| $3\frac{11}{16}$ | 0.3073 | $7\frac{11}{16}$ | 0.6406 | $11\frac{11}{16}$ | 0.9740 | $\frac{59}{64}$ | 0.921875 |
| $3\frac{3}{4}$ | 0.3125 | $7\frac{3}{4}$ | 0.6458 | $11\frac{3}{4}$ | 0.9792 | $\frac{15}{16}$ | 0.9375 |
| $3\frac{13}{16}$ | 0.3177 | $7\frac{13}{16}$ | 0.6510 | $11\frac{13}{16}$ | 0.9844 | $\frac{61}{64}$ | 0.953125 |
| $3\frac{7}{8}$ | 0.3229 | $7\frac{7}{8}$ | 0.6563 | $11\frac{7}{8}$ | 0.9896 | $\frac{31}{32}$ | 0.96875 |
| $3\frac{15}{16}$ | 0.3281 | $7\frac{15}{16}$ | 0.6615 | $11\frac{15}{16}$ | 0.9948 | $\frac{63}{64}$ | 0.984375 |
| 4- | 0.3333 | 8- | 0.6667 | 12- | 1.0000 | 1" | 1.000 |

WHERE ADDITIONAL LUMBER INFORMATION MAY BE OBTAINED

THIS publication is a part of the service to distributors and consumers of lumber sponsored by the National Lumber Manufacturers Association. It is suggested that those desiring additional information regarding the respective species of wood write the following regional associations:

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| American Walnut Manufacturers Association..... | Chicago, Ill. |
| American Walnut. | |
| Appalachian Hardwood Manufacturers, Inc..... | Cincinnati, O. |
| Appalachian Ash, Basswood, Beech, Birch, Butternut, Chestnut, Cherry, Elm, Hickory, Maple, Yellow Poplar, Red Oak, White Oak, Walnut. | |
| Hardwood Dimension Manufacturers Association..... | Louisville, Ky. |
| American Walnut, Ash, Basswood, Beech, Birch, Butternut, Chestnut, Cherry, Elm, Hickory, Maple, Yellow Poplar, Red Oak, White Oak, Hemlock, Tamarack, White Pine, Cypress (yellow), Cottonwood, Gum (black), Gum (red and sap), Hackberry, Magnolia, Pecan, Persimmon, Sycamore, Tupelo, Willow. | |
| Mahogany Association, Inc..... | Chicago, Ill. |
| Mahogany. | |
| Maple Flooring Manufacturers Association..... | Chicago, Ill. |
| Maple, Beech and Birch Flooring. | |
| Northeastern Lumber Manufacturers Association..... | New York, N. Y. |
| Northern White Pine, Norway Pine, Eastern Spruce, Balsam Fir, Northern Hardwoods. | |
| Northern Hemlock and Hardwood Manufacturers Association..... | Oshkosh, Wis. |
| Hemlock, Birch, Maple, Basswood, Elm, Ash, Beech, Tamarack, White Pine. | |
| Northern Pine Manufacturers Association..... | Minneapolis, Minn. |
| Northern White Pine, Norway Pine, Eastern Spruce, Tamarack. | |
| Red Cedar Shingle Bureau..... | Seattle, Wash. |
| Red Cedar Shingles. | |
| Southern Cypress Manufacturers Association..... | Jacksonville, Fla. |
| Tidewater Red Cypress. | |
| Southern Hardwood Producers, Inc..... | Memphis, Tenn. |
| Ash, Basswood, Beech, Cypress (yellow), Cottonwood, Elm, Gum (black), Gum (red and sap), Hackberry, Hickory, Maple (soft), Magnolia, Oak (white), Oak (red), Poplar, Pecan, Persimmon, Sycamore, Tupelo, Willow. | |
| Southern Pine Association..... | New Orleans, La. |
| Longleaf and Shortleaf Southern Pine. | |
| West Coast Lumbermen's Association..... | Seattle, Wash. |
| Douglas Fir, West Coast Hemlock, Sitka Spruce, Western Red Cedar, Port Orford Cedar. | |
| Western Pine Association..... | Portland, Ore. |
| Ponderosa Pine, Idaho White Pine, Sugar Pine, Larch, Douglas Fir, White Fir, Engelmann Spruce, Red Cedar, Incense Cedar. | |
| The Veneer Association..... | Chicago, Ill. |

NATIONAL LUMBER MANUFACTURERS ASSOCIATION

1337 Connecticut Ave., Washington, D. C.

FIELD OFFICES

Chicago

New York

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COOPERATING ORGANIZATIONS

| | |
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| National Hardwood Lumber Association..... | Chicago, Ill. |
| National-American Wholesale Lumber Association..... | New York, N. Y. |
| National Retail Lumber Dealers Association..... | Washington, D. C. |
| National Association of Commission Lumber Salesmen..... | Cleveland, O. |
| National Door Manufacturers Association..... | Chicago, Ill. |
| National Association of Hardwood Wholesalers..... | Chicago, Ill. |
| National Wholesale Lumber Distributing Yard Association..... | Baltimore, Md. |

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| National Hardwood Lumber Association..... | Chicago, Ill. |
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